19 March 2019

AGUIA REPORTS MAIDEN RESOURCE ESTIMATE FOR ANDRADE COPPER DEPOSIT

Highlights:

- **Total Inferred Mineral Resource estimate is 10.8 million tonnes with an average grade of 0.56% copper and 2.56 grams/tonne silver**
- **Mineral Resource Statement includes:**
  - **An open pit-constrained Inferred Resource of 1.3 million tonnes of oxidized material, from surface, grading 0.43% copper**
  - **8.8 million tonnes of sulphide-bearing material grading 0.51% copper**
  - **675 thousand tonnes of sulfide-bearing material, amenable for underground mining, grading 1.42% copper**
- **CIM and JORC Compliant Mineral Resource for Andrade to be expanded with future drilling**
- **Três Estradas community consultations taking place later this month**

SYDNEY, AUSTRALIA March 19, 2019 - Brazilian mineral resource developer Aguia Resources Limited (ASX: AGR, TSXV: AGRL) (“Aguia” or the “Company”) is pleased to report the maiden resource for the recently acquired Andrade copper deposit, part of the Primavera Project, in Rio Grande do Sul, Brazil. The entire dataset was subject to independent review and audit by Toronto based firm Roscoe Postle Associates Inc. (RPA) which has signed off on the new resource statement for the project (the “Mineral Resource Statement”). The resource estimate meets the criteria required to be compliant with both JORC and CIM standards.

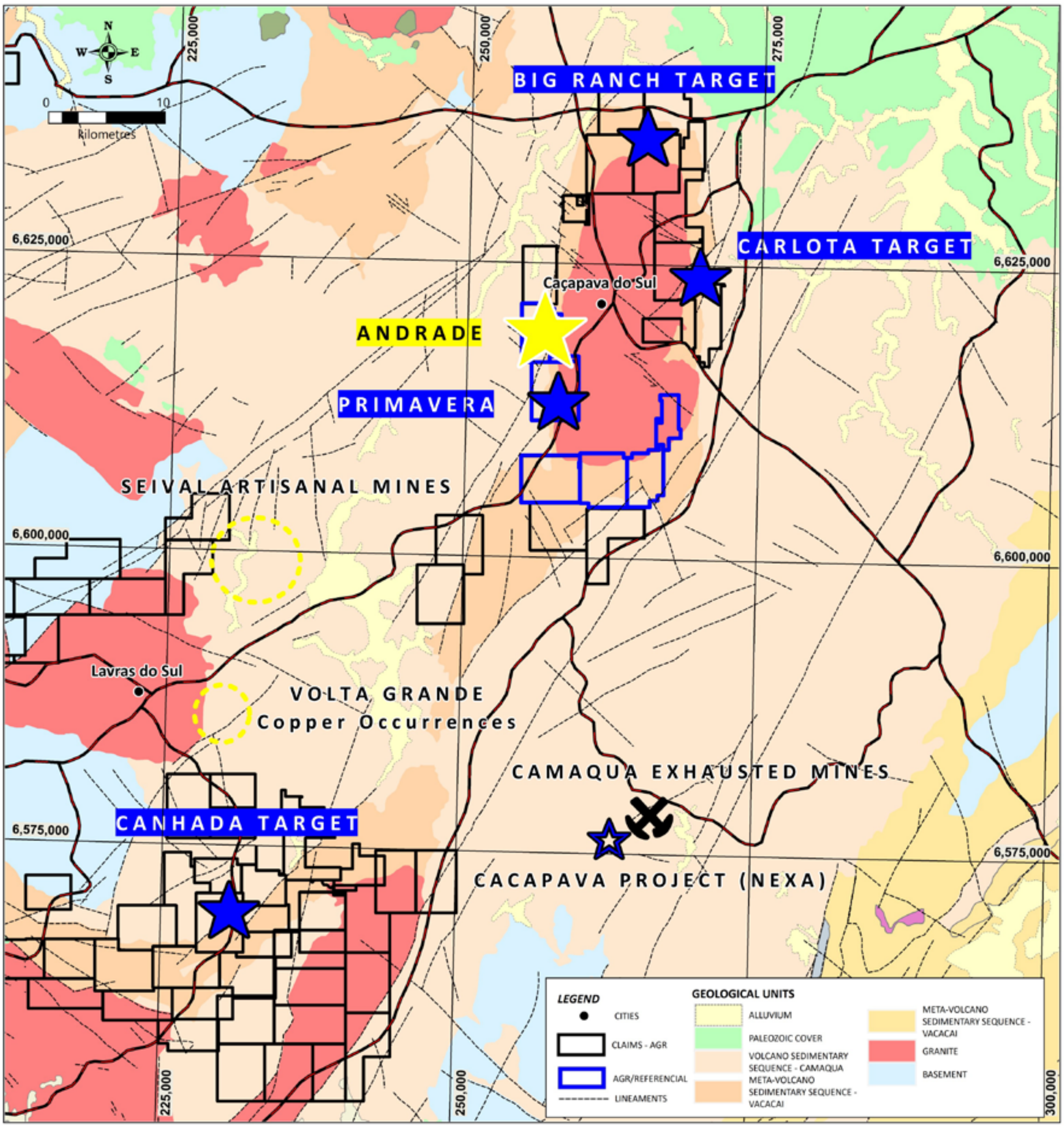


Figure 1. Geological map of the Rio Grande Copper Belt showing Aguia's existing claims at Big Ranch and Canhada in relation to the new claims recently acquired from Referencial which are outlined in blue.

The Mineral Resource Statement is based on the results of 38 historical diamond drill holes drilled by Referencial Geologia Ltda. (Referencial) between 2009 and 2010 that were compiled and integrated into the database together with a drilling campaign carried out by Aguia in January and February 2019 as part of the due diligence the Company undertook before signing the option to acquire the Primavera Project from Referencial (see ASX release 28 February 2019). During this period, Aguia completed three drill holes (382 m). The primary goal of this drilling campaign was to confirm the presence of significant copper intersections that would suggest economic potential. The drilling campaign was successful as assay results from all three drill holes returned thick and high-grade zones of copper mineralisation, which has provided the data needed for a maiden resource that is JORC and CIM (as incorporated in NI 43-101) compliant.

The Mineral Resource Statement includes an open pit-constrained Inferred Resource of 1.3 million tonnes of oxidized material, from surface, grading 0.43% copper and 8.8 million tonnes of sulphide-bearing material grading 0.51% copper, and an additional 675 thousand tonnes of sulfide-bearing material, amenable for underground mining, grading 1.42% copper. The total Inferred Mineral Resource is 10.8 million tonnes with an average grade of 0.56% copper and 2.56 grams per tonne of silver. See details of the CIM / JORC-compliant mineral resource statement in the table below and the attached Material Information Summary and JORC Table 1.

TABLE 1 – AGUIA RESOURCES – ANDRADE DEPOSIT- MARCH 13, 2019

		Tonnes (kt)	Cu Grade (%)	Ag Grade (g/t)	Cu (kLb)	Ag (kOz)
Oxide	Open Pit	1,337	0.43	2.54	12,778	109
Sulphide	Open Pit	8,796	0.51	2.15	98,525	607
	Underground	675	1.42	8.06	21,185	175
TOTAL INFERRED MINERAL RESOURCES		**10,807**	**0.56**	**2.56**	**132,488**	**891**

1. Mineral Resources conform to the standards set out by CIM (2014) and JORC Code (2012)
2. Open pit resources are stated within a Whittle pit shell, above a cut-off grade of 0.2% Cu
3. Underground resources are reported above a cut-off grade of 1% Cu
4. Cut-off grades were calculated using a copper price of US$3.50/lb and a silver price of US$20/oz
5. Average bulk densities of 2.68 t/m^3 for high grade domains and 2.6 t/m^3 for low grade and waste domains were applied
6. Resources are reported on a 100% basis. No mining loss or mining dilution factors have been applied to the reported figures.
7. Mineral Resources are not Ore Reserves and should not be considered as such. They do not have demonstrated economic viability
8. Totals may not sum due to rounding

Technical Director Dr. Fernando Tallarico commented: “This first pass drilling campaign at Andrade was very successful and provided us with the key data we needed to proceed with the option to acquire the Primavera Targets. Based on the historical data available to us, it became clear that Andrade was a priority target for our initial drilling. The available data allowed us to define a small maiden Inferred Mineral Resource exceeding 10 million tonnes - a great foundation for further exploration that we expect will expand this Mineral Resource Estimate. We are eager to ramp up drilling as quickly as we can.”

Managing Director Justin Reid added: “Andrade is the jewel in the crown of the Primavera Project claims we recently acquired. The new Mineral Resource for Andrade is located in a single structural panel. We have identified at least four panels over an 8 km strike which starts north of Andrade and ends 2 km to the south of Primavera. This will be our area of focus of our copper exploration efforts going forward with the intention to add to the current Mineral Resource as we gather more drilling data. We believe these recent developments have the potential to create significant value and we are actively engaged on a means of effectively delivering this value to shareholders.”

“2019 is also off to an exciting start for Aguia’s Três Estradas Phosphate Project as we approach the community consultation on March 20, 2019; one of the final conditions to be completed for the granting of the environmental permit. Obtaining this permit will mark a major de-risking event for Aguia and advances the Company to the next stage of development to become a phosrock producer.”

TABLE 2: SENSITIVITY ANALYSIS OF THE ANDRADE RESOURCE AT DIFFERENT CUT-OFF GRADES

	Cut-off Grade (%Cu)	Tonnes (kt)	Cu Grade (%)	Ag Grade (ppm)	Cu (klb)	Ag (koz)
OP	**0.2**	**10,133**	**0.50%**	**2.20**	**111,304**	**716**
	0.4	3,947	0.79%	2.90	69,136	368
	0.6	1,369	1.40%	4.96	42,138	218
	0.8	791	1.93%	7.28	33,704	185
	1.0	724	2.03%	7.62	32,423	177
	1.5	643	2.11%	8.02	29,897	166
UG	**1.0**	**675**	**1.42%**	**8.06**	**21,185**	**175**
	1.5	156	1.69%	7.61	5,798	38

Notes:

1. Open pit resources are reported on a whole block basis, above the pit optimization shell as detailed above.

Competent/Qualified Persons

The Mineral Resource estimate was prepared in accordance with the standards set out in both the 2012 edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves' (JORC Code) and with Canadian Institute of Mining, Metallurgy and Petroleum (CIM) definitions as incorporated in National Instrument 43-101 – Standards of Disclosure for Mineral Projects of the Canadian Securities Administrators ("NI 43-101"). The JORC Code is the accepted reporting standard for the Australian Stock Exchange Limited ("ASX").

The scientific and technical information contained in this news release pertaining to the Mineral Resource estimate on the Andrade copper deposit has been reviewed and approved by Mr. John Makin, MAIG, a Senior Geologist at Roscoe Postle Associates Inc. Mr. Makin qualifies as a Competent Person as defined in the JORC Code and a Qualified Person as defined by NI 43-101. He is independent of the Company at the time of this report. The results of the Mineral Resource Statement will be described in greater detail in the NI43-101 compliant technical report to be subsequently filed on SEDAR in accordance with applicable securities laws.

For further information, please contact:

Justin Reid, Managing Director
E: jreid@aguiaresources.com.au
T: **+1 416-216-5446**

Spyros Karellas, Investor Relations North America
E: spyros@pinnaclecapitalmarkets.ca
T: +1 416-433-5696

Released through: Ben Jarvis, Six Degrees Investor Relations: +61 413 150 448

Follow Aguia on Twitter: @ Aguia_Resources

About Aguia:

Aguia Resources Limited, ("Aguia") is an ASX and TSX Venture listed company whose primary focus is on the exploration and development of mineral resource projects in Brazil. Aguia has an established and highly *experienced in-country team based in Belo Horizonte, Brazil with corporate offices in Sydney, Australia. Aguia's key projects are located in Rio Grande do Sul, a prime farming area which is 100% dependent on phosphate imports. The Rio Grande phosphate deposits exhibit high quality and low cost production characteristics, and are ideally located with proximity to road, rail, and port infrastructure. Aguia's experienced management team has a proven track record of advancing high quality mining assets to production in Brazil.*

Cautionary Statement on Forward Looking Information

This press release contains "forward-looking information" within the meaning of applicable Canadian and Australian securities legislation. Forward-looking information includes, without limitation, statements regarding the results of the Mineral Resource Statement, the mineral resource estimates, production targets, the anticipated timetable, permitting, forecast financial information, bankable feasibility study and ability to finance the project, and the prospectivity and potential of the Andrade target within the Primavera Project claims.

Generally, forward-looking information can be identified by the use of forward-looking terminology such as "plans", "expects" or "does not expect", "is expected", "budget", "scheduled", "estimates", "forecasts", "intends", "anticipates" or "does not anticipate", or "believes", or variations of such words and phrases or state that certain actions, events or results "may", "could", "would", "might" or "will be taken", "occur" or "be achieved". The material factors and assumptions underlying the forward-looking information of the Mineral Resource Statement results have been outlined above and will be detailed in the associated technical report.

Forward-looking information is subject to known and unknown risks, uncertainties and other factors that may cause the actual results, level of activity, performance or achievements of the Company to be materially different from those expressed or implied by such forward-looking information, including risks inherent in the mining industry and risks described in the public disclosure of the Company which is available under the profile of the Company on SEDAR at www.sedar.com*, on the ASX website at www.asx.com.au and on the Company's website at www.aguiaresouces.com.au. These risks should be considered carefully.*

Although the Company has attempted to identify important factors that could cause actual results to differ materially from those contained in forward-looking information, there may be other factors that cause results not to be as anticipated, estimated or intended. Persons reading this news release are cautioned that such statements are only predictions and there can be no assurance that such information will prove to be accurate, as actual results and future events could differ materially from those anticipated in such statements. Accordingly, readers should not place undue reliance on forward-looking information. The Company disclaims any intent or obligation to update or revise any forward looking statements whether as a result of new information, estimates, options, future events, results or otherwise and does not undertake to update any forward-looking information, except in accordance with applicable securities laws.

NEITHER THE AUSTRALIAN STOCK EXCHANGE, TSX VENTURE EXCHANGE NOR THEIR REGULATION SERVICES PROVIDER (AS THAT TERM IS DEFINED IN THE POLICIES OF THE TSX VENTURE EXCHANGE) ACCEPTS RESPONSIBILITY FOR THE ADEQUACY OR ACCURACY OF THIS RELEASE.

MATERIAL INFORMATION SUMMARY

A Material Information Summary pursuant to ASX Listing Rule 5.8 is provided below for the Andrade deposit Mineral Resource estimate. The Checklist of Assessment and Reporting Criteria (Table 1) in accordance with the JORC Code (2012) is presented in Appendix A.

PROPERTY DESCRIPTION

The Andrade deposit is located in the central southern region of the state of Rio Grande do Sul, Brazil. The project is near the town of Caçapava do Sul, approximately 230 km from the state capital, Porto Alegre (Figure 1). The project area is easily reached via federal highways and local roads and is well served with critical infrastructure in the region.

The local climate is mild with daily average temperatures ranging from 12 ºC in July to 24 ºC in January. Rainfall is consistent year-round with monthly average rainfall ranging from 111 mm in December to 142 mm in July.

Extractive industries have a long history in the area; historical mining for copper occurred at Camaqua and limestone quarrying is currently a major employer in the town. At the Andrade deposit, historic investigations include the digging of an 18 m shaft and a 23 m adit in the early 1900s, and extensive trenching and sporadic drilling programs carried out by the government mines department. These historical programs were not used in the estimation of this Mineral Resource.

GEOLOGY AND GEOLOGICAL INTERPRETATION

The local geology of the Andrade deposit can be grouped into three main units (Figure 2). The central meta-volcanic package, identified as part of the Vacacaí Metamorphic Complex, varies from a more mafic meta-basalt unit in the west to intermediate meta-andesites and meta-dacites on its west flank. The meta-dacites and meta-andesites host the Cu-Ag enrichment that forms the Andrade deposit. To the west, this meta-volcanic package is unconformably overlain by the sedimentary conglomerates of the Santa Bárbara Formation; the contact between the units is documented as both erosive and faulted. In the east, the meta-volcanic rocks were intruded by the Caçapava granite and this unit dominates the eastern flank of the area of interest. This unit is interpreted to be the source of the mineralizing fluids that formed the Andrade deposit.

The primary mineral assemblage of economic interest at Andrade consists of bornite, chalcocite and, more rarely, chalcopyrite. These occur as disseminated sulphides through the mineralized zone. Higher grade zones are present as more massive sulphide aggregations, typically associated with the selvages of carbonate veining.

The near surface expression of mineralization in the oxide zone is dominated by malachite and chrysocolla with minor cuprite and tenorite also found.

FIGURE 1 PROJECT LOCATION MAP

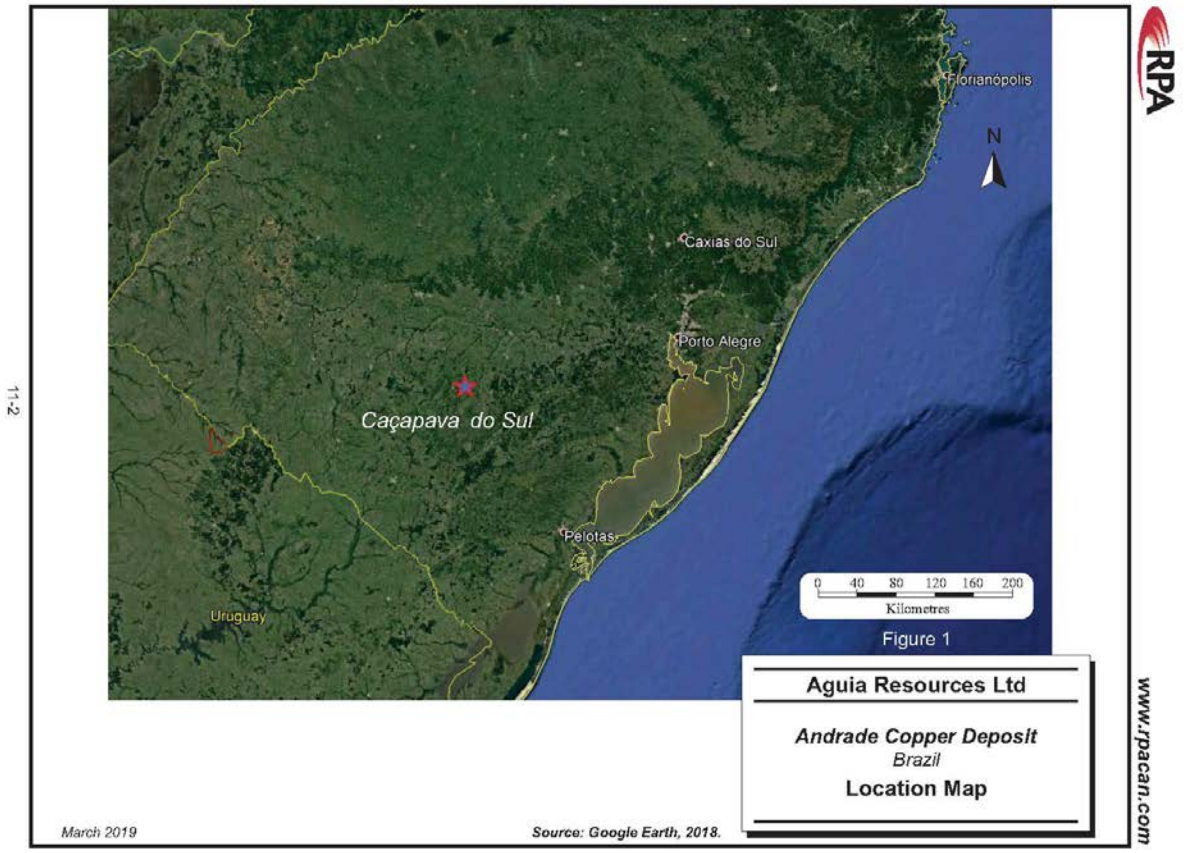
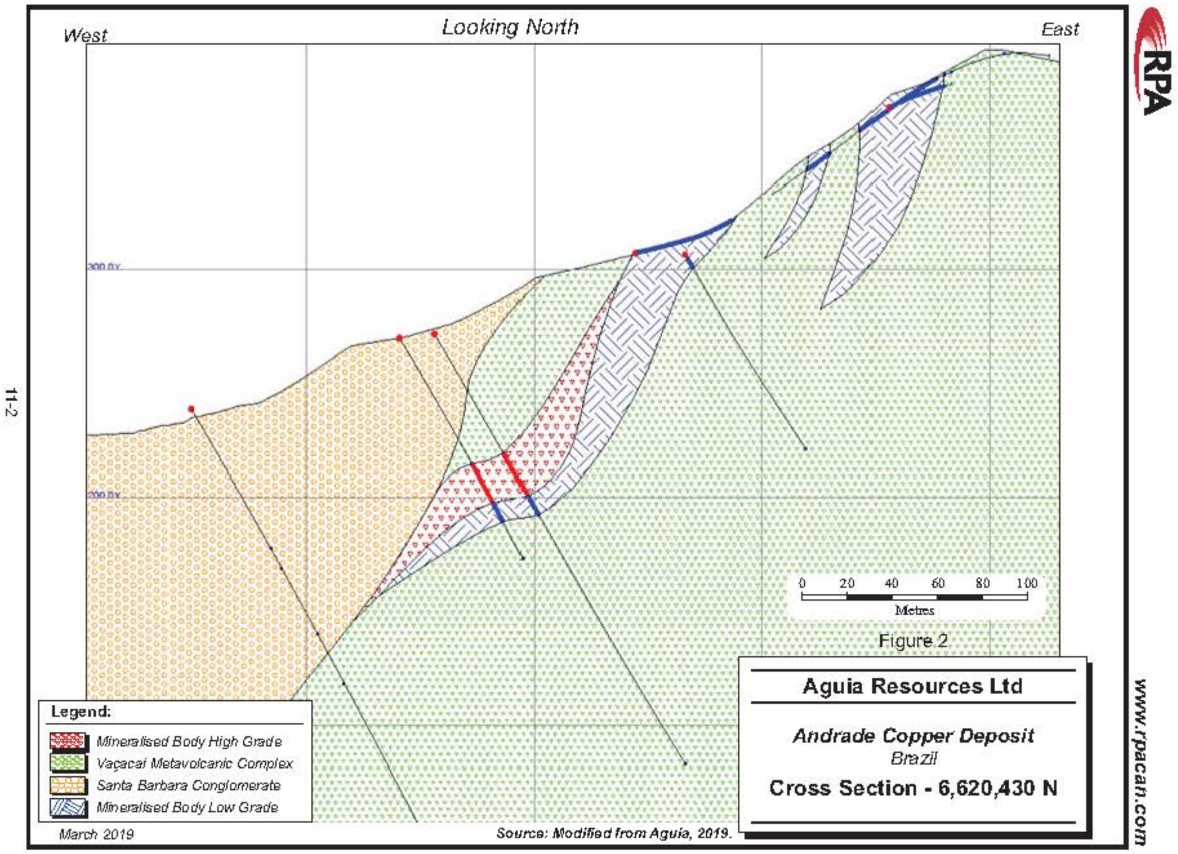


FIGURE 2 SCHEMATIC GEOLOGY CROSS SECTION



Source: Modified from Aguia, 2019.

DRILLING TECHNIQUES

The Mineral Resource estimate at Andrade has been informed by 38 diamond core drill holes completed by Referencial Geologia Ltda. (Referencial), for a total of 8,406 m of drilled core. Aguia Resources Ltd (Aguia) drilled three confirmation holes (382.4 m) in 2019 as part of their due diligence program. These drill holes were used to guide the wireframe construction but were not included in the grade estimate as assays had not been received before the data cut-off for estimation (Figure 3).

Diamond core was drilled at HQ size through the weathered zone, reducing to NQ size once the bedrock was reached.

All drill hole collars were surveyed using differential global positioning system (GPS) and down hole surveys were carried out at three metre intervals using a Maxibor optical down hole survey tool.

A total of 19 historical trenches were re-sampled by Referencial. The results of this program were used in the estimation of the near surface oxide zone but were restricted from influencing the sulphide estimates.

SAMPLING AND SUB-SAMPLING TECHNIQUES

Drill core sample lengths range from 0.5 m to 1.6 m with an average sample length of one metre. Drill core was sawn into half core lengths and sent for preparation at ALS laboratory in Belo Horizonte, Brazil.

Historic trenching works were comprehensively re-sampled by Referencial in 2009 and 2010. Samples were collected as one metre long channels from the trench wall and totalled 1,088 m in length.

All samples were dried, crushed, and milled to 70% passing 2 mm, riffle split off 250 g, then the split pulverised to better than 85% passing 75 microns.

SAMPLE ANALYSIS METHODS

Assays were conducted by ALS Peru S.A. All samples were analyzed for a 33 element package using a four acid ‘near total’ digestion with inductively coupled plasma atomic emission spectrometry (ICP-AES) finish. Over limit results for Cu and Co were re-analyzed by four acid digestion, HCl leach and ICP finish.

Quality control samples were routinely inserted into the sample stream in accordance with current industry practices. Quality control and quality assurance (QA/QC) measures included the insertion of certified reference materials (CRM), blank material, field and pulp duplicates, and periodic check assays using a second laboratory.

ESTIMATION METHODOLOGY

Two domains were modelled separating low- and high-grade lenses of mineralization (Figure 4). The low-grade domain was additionally divided into fresh rock and weathered zones.

FIGURE 3 SURFACE GEOLOGY PLAN WITH DRILL HOLE COLLARS

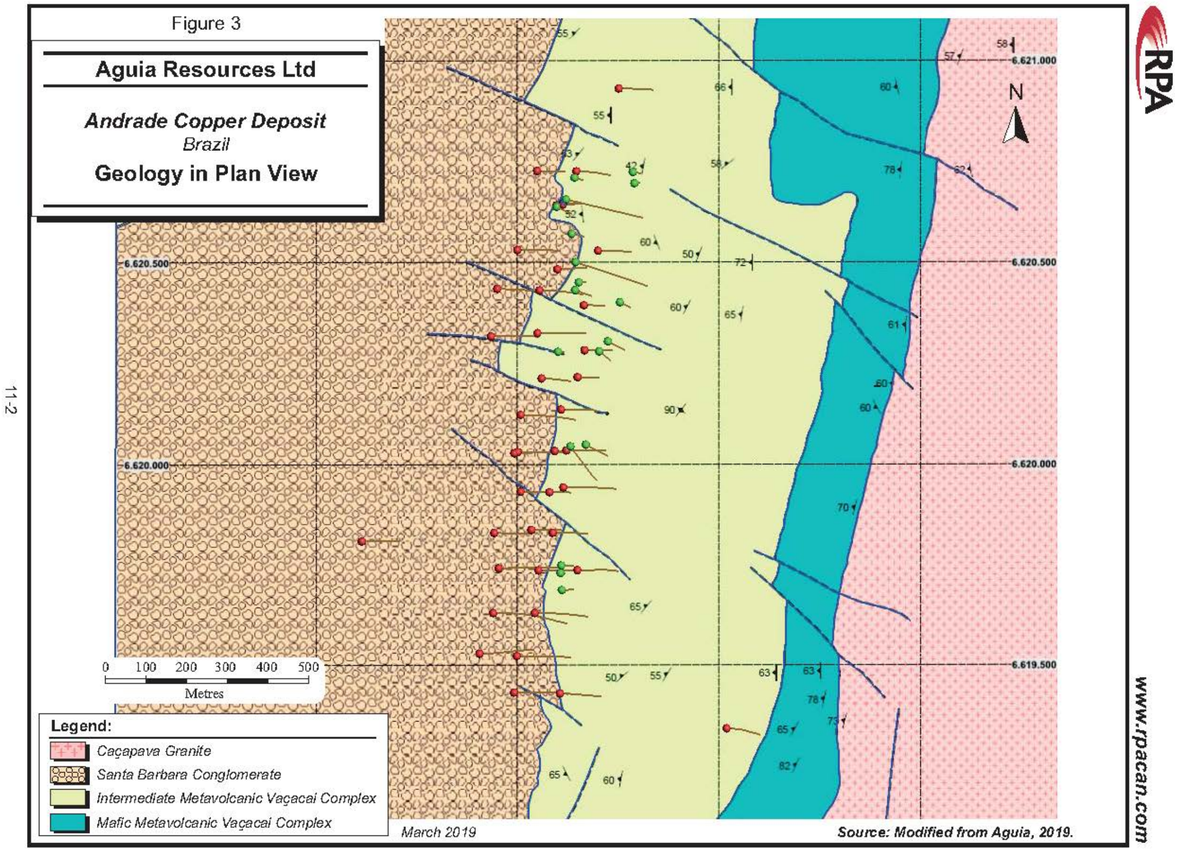
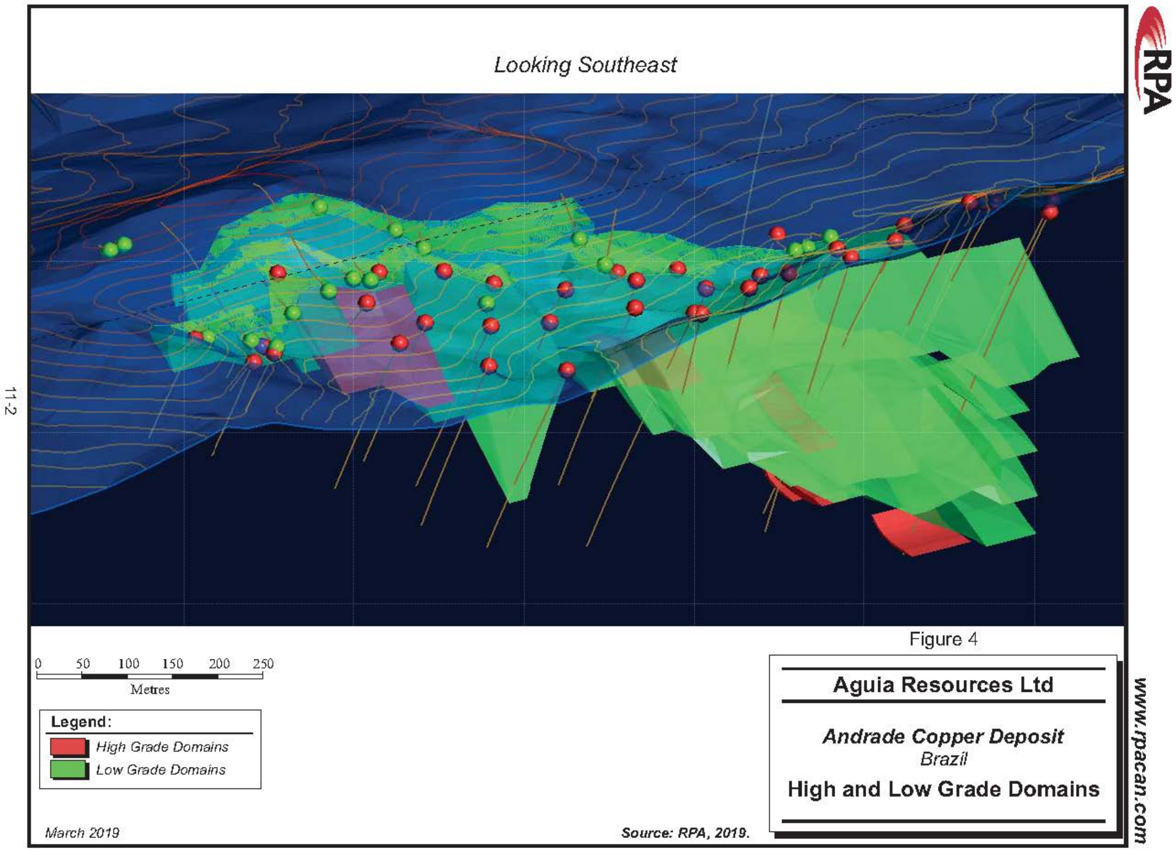


FIGURE 4   OBLIQUE VIEW OF ESTIMATION DOMAINS WITH TOPOGRAPHY



Assays were composited to one metre intervals and a capping value of 20 g/t Ag was applied to silver assays. No capping was considered necessary for copper assays.

Variogram models were fitted to the composite data, and Cu and Ag grades were estimated into a three-dimensional block model using ordinary kriging within Geovia's GEMS software. The selected block size was 5 m x 5 m x 5 m and the estimation was constrained to whole blocks within the mineralized wireframe domain models. Block estimations were calculated in two search passes using progressively larger search ellipse ranges and more relaxed selection criteria.

MINERAL RESOURCE CLASSIFICATION

All estimated blocks, above the cut-off grade, are reported as Inferred Mineral Resources. The wide spaced nature of the drilling (100 m x 100 m) precludes the declaration of an Indicated Mineral Resource.

MINING, METALLURGICAL AND MODIFYING FACTORS

In order to demonstrate reasonable prospects for eventual economic extraction, a conceptual operating scenario was designed for a 1 million tonnes per annum (Mtpa) production rate. This allowed the estimation of basic mining, processing, and general and administration (G&A) costs.

Open pit assumptions included a mining cost of US$4/t, processing cost of US$12/t and a G&A cost of US$1/t. For underground mining methods, the cost assumptions were US$30/t for mining, US$15/t for processing, and US$3.75/t for G&A costs. The open pit resources were reported within a Whittle pit optimization shell (Figure 5) based on the above input costs and a pit slope angle of 55°.

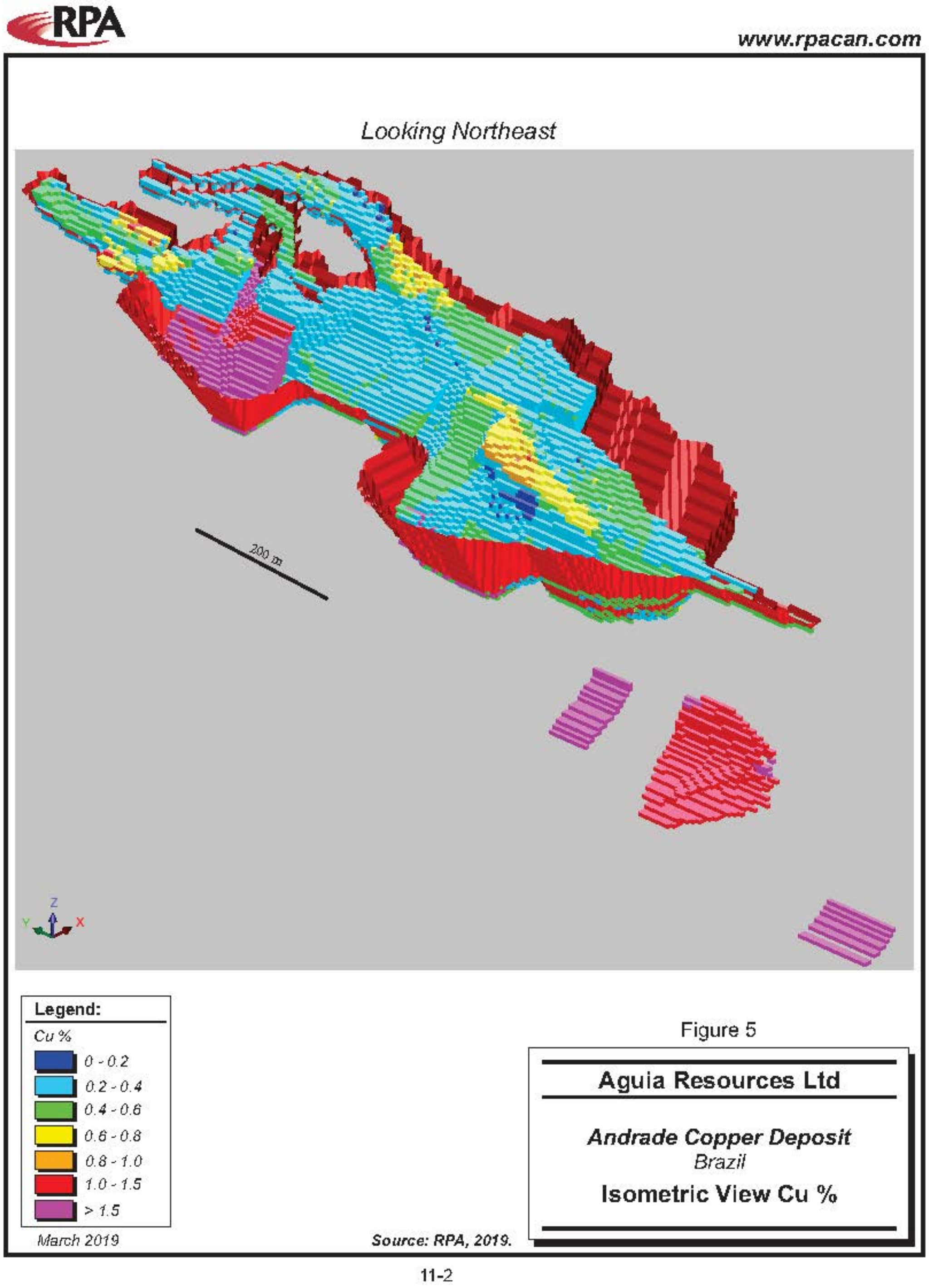
Costs of sales for copper and silver were set at US$0.10/lb of copper and US$0.50/oz of silver.

The input cost assumptions above were based on the experience of both Aguia and RPA and compared with operations of similar size within the greater region.

Commodity price assumptions were set at US$3.50/lb of copper and US$20/oz of silver.

Metallurgical recovery assumptions were based on a preliminary metallurgical recovery study carried out at the Federal University of Rio Grande do Sul. This study indicated that recoveries of 88% copper and 40% silver could be expected from concentration practices considered standard within the mining industry.

FIGURE 5 OBLIQUE VIEW SHOWING PIT OPTIMIZATION AND BLOCKS ABOVE CUT-OFF GRADE



CUT-OFF GRADES

The above cost assumptions were used to calculate cut-off grades, in order to state Mineral Resources at the Andrade deposit.

Open pit Mineral Resources are reported as blocks above a cut-off grade of 0.2% Cu, within the Whittle open pit optimization shell, based on the stated parameters above.

Underground Mineral Resources are stated above a cut-off grade of 1% Cu, based on the cost assumptions stated above.

MINERAL RESOURCES

The Inferred Mineral Resource estimate at the Andrade deposit is set out in Table 1 below.

TABLE 1 INFERRED MINERAL RESOURCES
Aguia Resources Ltd – Andrade Copper Deposit

		Tonnes (kt)	Cu Grade (%)	Ag Grade (g/t)	Cu (klb)	Ag (koz)
Oxide	**Open Pit**	1,337	0.43	2.54	12,778	109
Sulphide	**Open Pit**	8,796	0.51	2.15	98,525	607
	Underground	675	1.42	8.06	21,185	175
TOTAL INFERRED MINERAL RESOURCES		10,807	0.56	2.56	132,488	891

Notes:

1. Mineral Resources conform to the standards set out by CIM (2014) and JORC Code (2012).
2. Open pit resources are stated within a Whittle pit shell, above a cut-off grade of 0.2% Cu.
3. Underground resources are reported above a cut-off grade of 1% Cu.
4. Cut-off grades were calculated using a copper price of US$3.50/lb and a silver price of US$20/oz.
5. Average bulk densities of 2.68 t/m^3 for high grade domains and 2.60 t/m^3 for low grade and waste domains were applied.
6. Resources are reported on a 100% basis. No mining loss or mining dilution factors have been applied to the reported figures.
7. Mineral Resources are not Ore Reserves and should not be considered as such. They do not have demonstrated economic viability.
8. Totals may not sum due to rounding.

TABLE 2 MINERAL RESOURCE SENSITIVITY TO CUT-OFF GRADE
Aguia Resources Ltd – Andrade Copper Deposit

	Cut-off Grade (%Cu)	Tonnes (kt)	Cu Grade (%)	Ag Grade (ppm)	Cu (klb)	Ag (koz)
OP	**0.2**	**10,133**	**0.50%**	**2.20**	**111,304**	**716**
	0.4	3,947	0.79%	2.90	69,136	368
	0.6	1,369	1.40%	4.96	42,138	218
	0.8	791	1.93%	7.28	33,704	185
	1.0	724	2.03%	7.62	32,423	177
	1.5	643	2.11%	8.02	29,897	166
UG	**1.0**	**675**	**1.42%**	**8.06**	**21,185**	**175**
	1.5	156	1.69%	7.61	5,798	38

Notes:

1. Open pit resources are reported on a whole block basis, above the pit optimization shell as detailed above.

APPENDIX A – JORC CODE (2012) TABLE 1

SECTION 1: SAMPLING TECHNIQUES AND DATA

Sampling Techniques	• The Andrade deposit was defined using diamond core drilling, and surface trench sampling. • Drilling comprised 38 diamond core drill holes performed by Referencial from 2009 / 2010 campaign (8,406.34 m) and three core drill holes completed by Aguia from 2019 (382.4 m). • 19 historical trenches were re-sampled by Referencial in 2009 and 2010 (1,088.46 m). • All borehole collars were surveyed according to the local UTM coordinate system (SAD 69, Zone 22S), using a differential GPS receiver once drilling had been completed. • Down hole surveys were completed using a Maxibore down hole survey tool, collecting orientation readings at three-metre intervals. • Core Drilling - The majority of sample intervals range between 0.5 m and 1.6 m, averaging 1.0 m and honour geological contacts. Samples consisted of half core and were collected from core cut lengthwise using a diamond saw. Three readings per metre were performed with a portable X-ray fluorescence (XRF) device in the drill holes completed by Aguia to guide the sampling. • Samples were sent to the ALS laboratory in Vespasiano, in Belo Horizonte, Brazil for preparation. Prepared samples were sent to ALS laboratory in Lima, Peru for assay.
Drilling Techniques	• Diamond drilling utilized HQ equipment for weathered material and NQ for fresh rock. • Down hole surveys were performed for all diamond core holes. • Down hole surveys were performed on three-metre intervals using a Maxibore down hole tool. A total of 41 core holes have down hole surveys. • No core orientation has been carried out.
Drill Sample Recovery	• Drill core recovery was measured and recorded on a drill run and sample basis. Core recovery exceeded 90% in more than 90% of all core borehole samples. • No relationship between sample recovery and grade has been observed.
Logging	• Core Drilling - Detailed geological logs on appropriate logging form were completed. All cores have been photographed dry before sampling. Logging included description of lithology and weathering. Logged characteristics may be either qualitative or quantitative depending on the data being recorded. • 38 drill holes with a total length of 8,406 m were logged and assayed. All drill holes and all intervals were logged. • Additional geotechnical logging was carried out in the core shed, observing the lithological contacts. Measurements were: Total Core Recovery (TCR), Rock Quality Designation (RQD), Intact Rock Strength (IRS), degree of weathering, shear, fracture angles, joint sets, joint surface roughness, Joint Wall Strength (JWS).

Sub-Sampling Techniques and Sample Preparation	• Core was sawn in half, with one half sent for assaying and one half being retained for reference. • Friable core was split down the centreline, using a spatula or similar tool, with half being retained and half sent for assaying. • All samples were dried, crushed, and milled to 70% passing 2 mm, riffle split off 250 g, then the split pulverized to better than 85% passing 75 microns. • Coarse crush reject splits are collected and retained in storage. • The sample preparation techniques meet industry standards and RPA considers them appropriate for the mineralization being investigated. • Quarter core field duplicate samples and reject split duplicates were assayed to ensure the representivity and repeatability of the results. Duplicate assay results show very good agreement between samples. • RPA considers that the core sample sizes are adequate for the grain size of the target mineralization sampled.
Quality of Assay Data and Laboratory Tests	• Sample preparation was completed at ALS Vespasiano laboratory in Belo Horizonte, Brazil, using standard crushing and pulverization techniques PREP-31and PREP-31b (rock and drill samples). Sample analysis was carried out by ALS Peru S.A. • ME-ICP61 (ICP-AES) for 33 elements was used for the 2009 drilling samples; ME-ICP61a for the 2010 campaign drilling samples. For the analyses of gold, the following method was used: Au-AA26 (2010 drilling samples). • Routine assays were conducted using a four acid ‘near total’ digestion with ICP-AES finish (ME-ICP61 process) to provide analysis for 33 elements (Ag, Al, As, Ba, Be, Bi, Ca, Cd, Co, Cr, Cu, Fe, Ga, K, La, Mg, Mn, Mo, Na, Ni, P, Pb, S, Sb, Sc, Sr, Th, Ti, Tl, U, V, W, Zn). All Cu and Co determinations were re-assayed by four acid (HF-HNO$_3$-HClO$_4$) digestion, HCl leach and ICP finish to provide an improved level of accuracy on these values (method ME-OG62). • It is the opinion of RPA that the sample analysis procedures are appropriate to the style of mineralization. • In each batch of samples to be dispatched to a certified laboratory, 15% would be reference samples (duplicates, various grade standards (CRMs), a gold standard, and blanks). In each batch of 40 samples, 34 would be samples and six would be reference samples (2 duplicates, 3 standards, and 1 blank). • At ALS Peru S.A., second core splits were analyzed for a suite of 33 elements as a field duplicate sample. • Blank samples were sent for preparation to ALS laboratory in Vespasiano, Brazil and for analysis to ALS Peru S.A. • Referencial used eight CRMs (standards) sourced from Geostats Pty Ltd (Geostats) in Perth, Australia and AMIS from Isando in South Africa. • 244 duplicate core samples (approximately 3%) were selected for assay according to the QA/QC sampling plan. • SGS Geosol Laboratórios Ltda., Belo Horizonte, Brazil, was selected as the umpire laboratory. A total of 723 samples from the 35 holes used for the resource estimate, were re-analyzed, including, seven pairs of duplicates. The samples selected were from the holes used in the resource estimate and were randomly selected; CRMs were inserted and the samples dispatched to the SGS Geosol laboratory. The samples sent were in the form of coarse reject from the samples initially submitted to ALS Peru S.A. • RPA reviewed the results of the quality control samples and found no evidence of any material bias. RPA considers that acceptable levels have been established for the mineralization type.

Verification of Sampling and Assaying	• Two twin boreholes were completed by Aguia. The assay results and mineralized intervals present good correlation with the original drill holes. • All core was logged by Referencial geologists and verified by Aguia geologists; data was entered digitally into a comprehensive database program. Electronic data was verified against paper logs and original assay certificates by RPA. • Assay data did not need to be adjusted.
Location of Data Points	• All borehole collars were surveyed according to the local UTM coordinate system (South American Datum 1969 – SAD69, Zone 22S), using differential GPS equipment once drilling had been completed. • Down hole survey measurements were taken every three metres using the Reflex Maxibor optical deviation instruments. • A topographic survey of the project area was completed using differential GPS technology. • The survey comprised 2 km^2, consisting of survey lines spaced 100 m apart. • The topographic survey generated contour lines at one-metre intervals in the mineralized area. Contour lines at five-metre intervals were obtained for the remaining area using advanced land observing satellite (ALOS). • RPA is of the opinion that the topographic survey data is adequate for a project at this stage of development.
Data Spacing and Distribution	• The diamond drilling was completed on sections spaced 100 m apart with two to three drill holes per section. Drill hole spacing within each section was also approximately 100 m. • RPA considers that the current spacing is sufficient to establish the required continuity of geology and grade for an Inferred Mineral Resource. • No material has been classified as a Measured or Indicated Mineral Resource, and Ore Reserves are not being stated. • Assay data was composited to one-metre length prior to resource estimation.
Orientation of Data in Relation to Geologic Structure	• All drill holes were planned to intercept the mineralisation perpendicular to its expected strike. RPA is of the opinion that this has not introduced any material bias to the sampling of the mineralization. • Secondary structures that may influence the geometry and grade of the mineralization can be identified and should be considered in future drilling campaigns.
Sample Security	• Chain of custody of all sample material was maintained by Referencial and Aguia. Drill core is transported to the logging facility by staff technicians for logging and sampling by the company geologists. Samples were stored in a secured facility in Caçapava do Sul until dispatch to the preparation laboratory by commercial freight transport. • The retained half of each drill core and the returned coarse sample reject splits are stored in a secure storage facility in Caçapava do Sul.
Audits or Reviews	• RPA reviewed the sample collection techniques, quality control procedures, sample storage facility, and data integrity as part of a site visit carried out from the January 21 to 24, 2019. RPA is of the opinion that all relevant data has been collected and stored in accordance with industry best practice standards and is suitable to support the estimation of a Mineral Resource.

SECTION 2: REPORTING OF EXPLORATION RESULTS

Mineral Tenement and Land Tenure Status	• The Andrade deposit as currently modelled is situated over three separate exploration tenements.
	• The majority of the deposit is situated in proceedings 810.636/2007 and 810.808/2008. These are currently held by Referencial. Aguia has signed an option agreement with Referencial to acquire these tenements (as disclosed in a press release dated 27/02/2019). Upon the conclusion of this acquisition, these tenements will be subject to a 1% net smelter return royalty to be paid to Referencial.
	• The remainder of the deposit and the potential along strike extensions of the deposit are located in proceeding 810.187/2018. This claim is held by Aguia Fertilizantes S.A., a subsidiary company of Aguia.
	• Independent legal advice prepared for Aguia by William Freire Advogados Associados indicates that:
	  • Aguia satisfies the requirements for operating a mine within 150 km of the territorial borders of Brazil (the 'Border zone').
	  • The tenements in question do not fall within conservation units or indigenous lands.
	  • Those tenements that are currently under application or awaiting a response from the relevant department are unlikely to be denied.
	  • There are no known impediments to obtaining a licence to operate in this area.

Exploration Done by Other Parties	• 1900-08 Artisanal Mining: Trenches, pits, shafts and drifts at Andrade and Primavera • 1942 DNPM: (8 holes) Resource 462 kt at 0.8% Cu at Andrade • 1942 DNPM: Resource 91 kt at 1.00% Cu and 29 kt at 1.74% Cu at Primavera • 1959 DNPM: (25 holes) Resource 560 kt at 0.7% Cu 100 kt at 1% Cu at Andrade and Primvera • 1975 CRM: (13 holes) 3.3 Mt at 0.43% Cu at Andrade • 1985 CBC: (8 holes) 502 kt at 0.55% Cu at Andrade • 2009-10 Referencial: drilling completed (38 holes) at Andrade • 2009 Referencial: drilling completed (11 holes) at Primavera • 2012-13 Referencial: Deeper IP (TITAN) 4 sections completed at Andrade and Primavera
Geology	• The Andrade deposit is located at the western flank of the Caçapava Granite. • The local geological mapping reveals the presence of three large geologic domains from the east to the west: 1) granitoids of the Caçapava do Sul Granitic Suite, which is in tectonic contact with the 2) basic meta-volcano-sedimentary unit (amphibolites) of the Vacacaí Metamorphic Complex, which grades to the intermediate to acid meta-volcano-sedimentary package (feldspar chlorite schists and quartz chlorite schists), which is both in tectonic and erosive contact with the 3) conglomeratic sediments of the Santa Bárbara Formation. • The same units described with respect to the Andrade deposit are also found in the Primavera target, since the latter is an extension to the south of the former. However, meta-sediments, meta-tuffs, and meta-rhyodacites belonging to the Vacacaí Metamorphic Complex, as well as intrusions of basic volcanic rocks, are also seen.

Drill Hole Information	• Drilling utilized for the resource estimate consists of 38 diamond core boreholes drilled by Referencial from the 2009/2010 campaigns (8,406.34 m) and 19 historical trenches re-sampled by Referencial in 2009/2010 (1,088.46 m). A drill hole summary is appended to this table (Appendix B). • 3 diamond core boreholes drilled by Aguia in 2019 (770 m) were not used in this estimate as assays were not available at the estimation date. These holes were used only to guide the interpretation of wireframes. These holes are documented in a previous media release, dated February 27, 2019.
Data Aggregation Methods	• No exploration data were altered. • Intercepts above 0.2% Cu are considered significant. • No metal equivalents have been reported.
Relationship Between Mineralization Widths and Intercept Lengths	• Core drilling was designed to intersect the full width of the copper mineralization at a high angle. • Drill holes do not typically intercept the mineralisation perpendicularly, hence down hole widths are greater than true widths. For boreholes drilled with a dip of 60°, true mineralization widths were generally in the order of 80% to 90% of down hole intersection lengths. • Down hole lengths were reported. Relationships between true lengths and true thickness are shown in cross sections within the release.
Diagrams	• Borehole collar map, representative section, and a table of significant intercepts is included in Appendix B.
Balanced Reporting	• Significant intercepts, as defined above, from the Referencial drilling program are tabulated in Appendix C below.
Other Substantive Exploration Data	• Aguia made use of an airborne magnetic geophysical survey completed by CPRM to aid in exploration targeting and an extensive geological mapping program developed by Referencial.
Further Work	• Further work at the Andrade deposit is initially focussed on replicating high grade intercepts found in historical drilling. These historical intercepts were not included in this Mineral Resource but have the potential to increase the grade and/or extend the high grade volumes of the deposit. • Geophysical exploration methods such as a moving loop ground electromagnetic (EM) survey and down hole geophysics will be undertaken at the Andrade deposit. The results of these programs will allow Aguia to better focus exploration drilling activities at Andrade and throughout the larger tenement package in the region. • Surface trenching will be used to test outcropping mineralization to the north of the known deposit extents. Further trenching will also take place at the Primavera target and will aim to close the distance between the two occurrences. • Diamond drilling will target extensions to the resource along strike and at depth and will additionally delineate the extents of high grade lenses that have already been defined. • Drilling will also source feeder material in order to carry out more comprehensive metallurgical test work and support the recovery parameters used in future resource estimations. • Further investigation into the structural framework at Andrade through surface mapping, sampling, and the subsequent integration of this into the geological model is also on-going.

SECTION 3: ESTIMATION AND REPORTING OF MINERAL RESOURCES

Database Integrity	• Assay data is provided to Aguia in spreadsheet form and directly copied to the company's data system. The database was provided to RPA in a digital format as a Microsoft Excel file. • Original assay certificates were provided to RPA and grades above 1% Cu were checked against the provided data set. A series of random spot checks were also carried out. The database was checked for overlapping samples, missing samples, and un-sampled intervals. RPA found no material issues with provided database and is of the opinion that it is suitable to support the estimation of a Mineral Resource.
Site Visits	• A site visit was undertaken by Mr. John Makin from January 21 to 24, 2019. Mr. Makin is a Senior Geologist with RPA and is an independent Competent Person for the purpose of JORC Code (2012). • RPA was given full access to the project site, relevant data, core storage facility, and Aguia's field offices in Caçapava do Sul. RPA was afforded full access to Aguia personnel and had in-depth conversations and meetings relating to past exploration work, data acquisition procedures, and future goals in project development.
Geological Interpretation	• RPA has confidence that the geological interpretation in cross section and along strike is robust enough to support the declaration of an Inferred Mineral Resource. • The deposit shows good continuity along strike and down dip in terms of both grade and lithology. • The geological model was built from the diamond drill hole and trench sample data as described in the previous sections. It used a lithological-assay based approach to define the boundaries of the copper mineralization and the following criteria: Minimum average grade of composite interval (hanging wall to footwall contact) is 0.20% Cu for low grade and 1.00% Cu for high grade. • Cross sectional interpretations of high grade (>1% Cu) and low grade (>0.2% Cu) mineralization lenses were undertaken. These were guided primarily by the host lithology and the assayed grade. The maximum length of internal dilution within a mineralized interval was four metres. These two-dimensional interpretations were then linked in Geovia's GEMS software using tie-lines to form three-dimensional mineralisation solids for block estimation. • A surface eight metres below the topography was used to define the oxidation horizon. • Some sub-vertical east-west faulting occurs within the deposit but the influence of these structures on the geometry of the deposit is not yet well understood.
Dimensions	• The Andrade deposit has been drilled along a strike length of 1,400 m. It plunges shallowly (approximately 20°) to the south and has been intercepted at depths of up to 550 m below surface. The general plane of the deposit dips at 60° to the west and has a width (in plan section) of up to 360 m from east to west.
Estimation and Modelling Techniques	• Two estimation domains were modelled, separating the low grade and high grade data populations. The low grade was divided in weathered and fresh rock by an eight-metre surface generated from the topography surface. Geovia's GEMS software was used to estimate grades into a 3D block model, constrained by mineralization wireframes. • Aguia composited all assay intervals to a length of one metre. Following top-cut analysis, 20 g/t Ag was selected as the high-grade limit. No cap was necessary for the copper estimate. • Omni-directional and down hole variography analysis was undertaken on one-metre composites for Cu and Ag for all domains combined. RPA considers that Aguia's calculation parameters, orientation, and fitted variogram models are

<table>
<tr><td></td><td>appropriate and reasonable given the available data and geological interpretation and suggest the use of variable direction variograms for future resource estimates.
• Cu and Ag were estimated into the block model using ordinary kriging within the mineralized domains. For all elements, two estimation passes were used with progressively relaxed search ellipsoids and data requirements. Block estimation required a minimum of four and a maximum of 12 samples in the first pass and a minimum of two and maximum of 12 samples in the second search pass. The estimation ellipse ranges and orientations are based on the variogram model for Cu.
• The block size of 5 m (along strike) by 5 m (perpendicular to strike) by 5 m (vertical) was used.
• RPA performed a visual validation of the block model by comparing block and borehole grades on a section by section basis. Aguia also produced a series of swath plots to compare kriging estimation and inverse distance squared (ID^2) with reasonable conformance. The resultant block estimates appear to be reasonable in comparison to the composite grades.
• RPA believes that the estimation methodology and parameters are appropriate for the estimation of an Inferred Mineral Resource.</td></tr>
<tr><td>Moisture</td><td>• All tonnage estimates in the model have been presented on a dry basis.</td></tr>
<tr><td>Cut-Off Parameters</td><td>• Open pit Mineral Resources are reported within a conceptual pit shell generated in Geovia’s Whittle software at a cut-off grade of 0.20% Cu. This was calculated based on input costs as detailed below and a uniform pit slope angle of 55°.
• Underground Mineral Resources are reported above a cut-off grade of 1.0% Cu. This was calculated based on the assumed costs as detailed below.</td></tr>
<tr><td>Mining Factors and Assumptions</td><td>• A basic operating scenario was designed based on a 1 Mtpa processing capacity and a 10-year mine life. This scenario was used to establish basic input cost assumptions that could be used to calculate cut -off grades. These cost assumptions are based on the experience of RPA and Aguia considering operations of similar size within the larger region. The operation is envisaged to utilize both open pit and underground mining methods.
<table>
<tr><th colspan="4">Input cost assumptions (USD)</th></tr>
<tr><th></th><th>Open Pit</th><th>Underground</th><th>Unit</th></tr>
<tr><td>Mining</td><td>4</td><td>30</td><td>$/t</td></tr>
<tr><td>Process</td><td>12</td><td>15</td><td>$/t</td></tr>
<tr><td>G&A</td><td>1</td><td>3.75</td><td>$/t</td></tr>
<tr><td>Cu Sales</td><td colspan="2">0.1</td><td>$/lb</td></tr>
<tr><td>Ag Sales</td><td colspan="2">0.5</td><td>$/oz</td></tr>
<tr><th colspan="4">Recovery (applied to both Sulphide and Oxide)</th></tr>
<tr><td>Cu</td><td colspan="2">88</td><td>%</td></tr>
<tr><td>Ag</td><td colspan="2">40</td><td>%</td></tr>
<tr><th colspan="4">Commodity Prices</th></tr>
<tr><td>Cu</td><td colspan="2">3.5</td><td>$/lb</td></tr>
<tr><td>Ag</td><td colspan="2">20</td><td>$/oz</td></tr>
</table></td></tr>
</table>

Metallurgical Factors and Assumptions	• Recovery assumptions above were based on a preliminary metallurgical study undertaken at the mineral processing laboratory at the Federal University of Rio Grande do Sul (UFRGS) in 2010. A Bond Ball Mill Work Index test was also carried out in 2010 at the Federal University of Rio de Janeiro (UFRJ). • Two samples, representative of different aspects of sulphide ore, were obtained from diamond drill core. The first, EM-001, was selected as representative of mainly disseminated mineralization predominant in the deposit. The second, EM-002, was selected as representative of mainly vein/replacement style mineralization seen to exist within the main body. A third sample, EM-003, was collected from trenches to represent oxidized material containing mainly malachite and chrysocolla. • The selected samples were used for a preliminary and non-conclusive work index, flotation, and leaching tests. • While these test results are small in scale and may not reflect achievable performance on a commercial scale, RPA believes that they are appropriate for use in a project at this stage of development.
Environmental Factors and Assumptions	• No environmental assessment study has been carried out to assess the likely environmental or social impacts of this project going into production. • No location or design studies have been undertaken to identify potential locations for tailings management facilities or waste rock storage. • RPA notes that the property is located in an area of current and historical mining activity.
Bulk Density	• Density was measured by Referencial on uncoated core samples using a standard weight in water/weight in air methodology, reporting values on a dry basis. The density database contains 696 measurements. • Density was applied to the block model as average values for high grade (2.68 t/m^3), low grade, and waste domains (2.60 t/m^3). • RPA and Aguia personnel identified that the values obtained by Referencial appear to be low for rock and mineralisation of this type. An initial cross-check program returned density values an average of 5% higher than the Referencial program. • Once density measurements have been confirmed by an independent laboratory, the modelled density can be updated. • The current values for density do not take into account the oxidation state or weathering profile. • RPA recommends that in future density should be estimated into the model rather than using assigned domain averages.
Classification	• All estimated blocks for the Andrade deposit are currently classified as Inferred. While the global geological continuity of the deposit appears to have been reasonably established, the variability in grade and local geometry cannot yet be ascertained. • The samples used to inform this estimate appear to be of good quality and have been collected and analyzed in accordance with standard industry practice, however, the wide spatial distribution (100 m x 100 m drill hole spacing) preclude any material from being considered as an Indicated or Measured Mineral Resource. • RPA believes that all relevant factors have been taken into account for the preparation of this Mineral Resource estimate. • It is the opinion of RPA that the Andrade Mineral Resource estimate appropriately reflects the Competent Person's view of the deposit.

Audits and Reviews	• RPA conducted a detailed review of the block model provided by Aguia and found no material issues in the estimation process or with the resulting model. • RPA believes that the model is of sufficient quality for the declaration of an Inferred Mineral Resource.
Discussion of Relative Accuracy/ Confidence	• The Mineral Resource at Andrade has been estimated using Industry standard procedures for a deposit of its nature. • Inferred Mineral Resources are not Ore Reserves and should not be considered for mine planning and scheduling purposes. They reflect a volume of mineralised material that requires significant further investigation before being able to be considered an Ore Reserve as defined by the JORC Code (2012). • The Mineral Resource estimate above is of the global tonnes and grade of the Andrade deposit as it is currently known. • No production data from the Andrade deposit is available as the historic artisanal mining activity was not documented.

SECTION 4: ESTIMATION AND REPORTING OF ORE RESERVES

No Ore Reserves are being reported.

SECTION 5: ESTIMATION AND REPORTING OF DIAMONDS AND OTHER GEMSTONES

Diamonds or other gemstones are not relevant to this report.

APPENDIX B: DRILL HOLE INFORMATION TABLE

HOLE-ID	Easting	Northing	RL	Max. Depth	Azimuth	Dip	Depth of First Significant Intercept
CPV_AN_DDH001	257114.30	6620642.01	271.53	83.81	87.00	-50.00	6.82
CPV_AN_DDH002	257099.02	6620640.05	266.05	90.60	87.00	-60.00	12.69
CPV_AN_DDH003	257123.20	6620032.32	248.84	150.00	87.00	-50.00	1.3
CPV_AN_DDH004	257100.70	6620481.50	297.64	119.90	87.00	-50.00	45
CPV_AN_DDH005	257081.07	6619926.28	217.68	171.00	90.00	-70.00	19.45
CPV_AN_DDH006	257168.09	6620280.71	287.62	110.90	90.00	-50.00	5.77
CPV_AN_DDH007	257089.22	6619825.56	213.23	238.40	90.00	-70.00	13
CPV_AN_DDH008	257109.89	6620133.57	248.70	137.90	90.00	-50.00	16
CPV_AN_DDH009	257036.43	6619832.71	226.78	237.00	90.00	-70.00	74.37
CPV_AN_DDH010	257166.28	6620392.41	306.78	100.90	90.00	-60.00	6
CPV_AN_DDH011	257150.84	6620213.93	263.47	101.90	90.00	-60.00	0
CPV_AN_DDH012	257053.53	6619732.32	234.90	180.00	90.00	-60.00	62.35
CPV_AN_DDH013	257061.61	6620210.75	231.65	150.00	90.00	-60.00	39.24
CPV_AN_DDH014	257009.74	6619927.49	230.80	216.00	90.00	-70.00	102.05
CPV_AN_DDH015	257093.88	6620030.73	243.95	170.00	90.00	-70.00	20.39
PRI_AN_DDH017	256613.99	6619803.91	313.05	277.15	90.00	-70.00	NSI
PRI_AN_DDH018	257520.27	6619340.87	312.08	278.35	90.00	-70.00	NSI
PRI_AN_DDH025	257107.10	6619427.05	227.23	201.05	90.00	-60.00	NSI
PRI_AN_DDH027	256939.22	6619626.40	291.20	434.35	90.00	-60.00	196.78
PRI_AN_DDH029	257044.32	6619626.56	245.58	249.05	90.00	-60.00	74.84
PRI_AN_DDH030	257056.30	6620428.96	271.84	218.75	90.00	-59.20	60.55
PRI_AN_DDH031	257150.40	6619732.99	235.35	203.85	90.00	-59.10	105
PRI_AN_DDH032	257252.87	6620929.92	359.62	184.70	90.00	-59.60	NSI
PRI_AN_DDH033	256905.58	6619525.71	267.71	504.35	90.00	-60.50	215.02
PRI_AN_DDH034	257201.24	6620527.39	323.88	164.90	90.00	-58.20	1
PRI_AN_DDH035	257000.09	6619519.89	263.07	247.58	90.00	-55.60	129.88
PRI_AN_DDH036	257001.63	6620529.15	274.76	223.50	90.00	-59.20	NSI
PRI_AN_DDH037	257147.88	6620724.49	289.70	161.80	90.00	-58.80	0
PRI_AN_DDH038	257050.41	6620725.26	278.84	143.85	90.00	-59.80	54

HOLE-ID	Easting	Northing	RL	Max. Depth	Azimuth	Dip	Depth of First Significant Intercept
PRI_AN_DDH039	256949.23	6620432.72	238.82	242.75	90.00	-59.70	126.5
PRI_AN_DDH040	256952.96	6619737.41	262.72	427.05	90.00	-59.30	164.75
PRI_AN_DDH041	256933.92	6620315.07	215.06	271.60	90.00	-60.10	155.7
PRI_AN_DDH042	257115.58	6619938.24	237.03	182.85	90.00	-42.30	0
PRI_AN_DDH043	257051.40	6620322.88	249.61	247.60	90.00	-59.60	54.67
PRI_AN_DDH044	257009.90	6620120.26	241.83	277.00	90.00	-59.00	66.95
PRI_AN_DDH045	256993.39	6619429.38	249.70	262.05	90.00	-58.21	134.35
PRI_AN_DDH047	256941.58	6619825.17	260.83	382.70	90.00	-68.18	190
PRI_AN_DDH049	257001.93	6620028.22	220.22	361.20	90.00	-58.80	86.44

APPENDIX C: DIAGRAMS AND LIST OF SIGNIFICANT INTERCEPTS

DRILLHOLE COLLAR PLAN

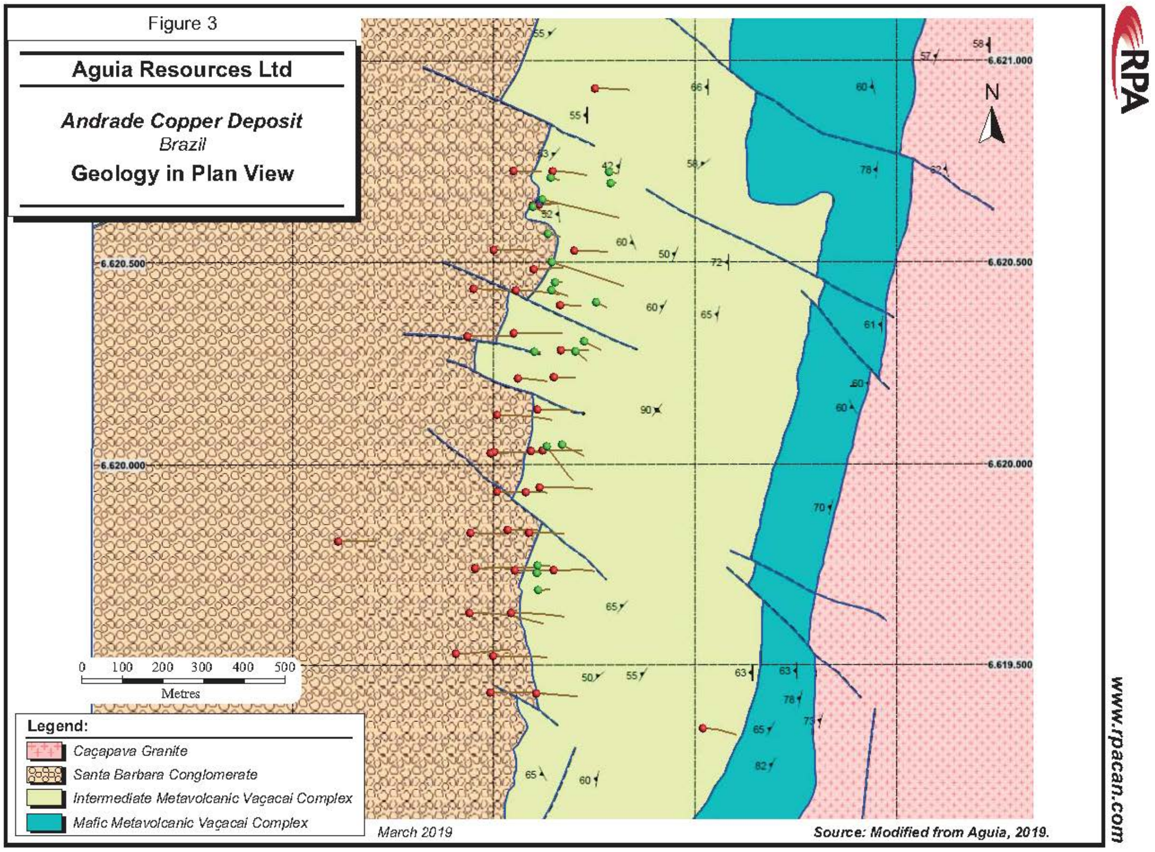


Figure 3

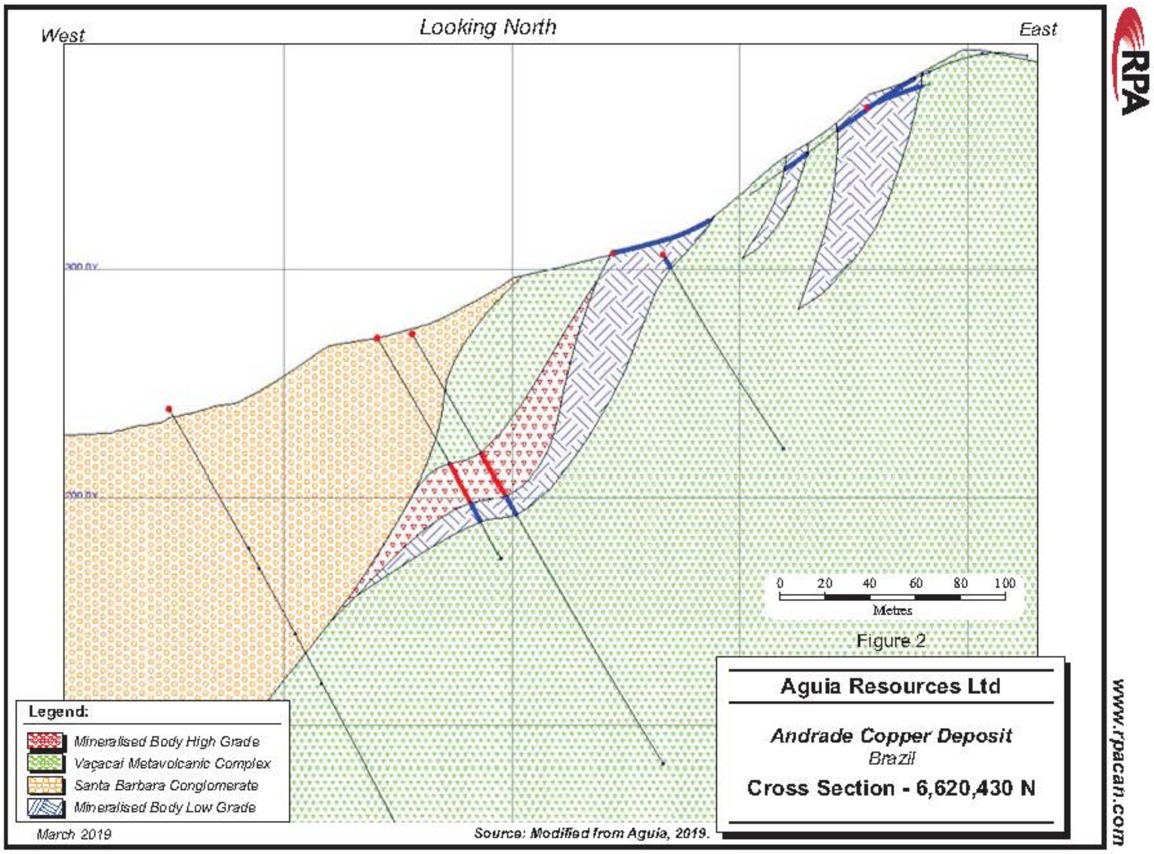
Aguia Resources Ltd

Andrade Copper Deposit
Brazil
Geology in Plan View

March 2019

Source: Modified from Aguia, 2019.

REPRESENTATIVE CROSS SECTION



SIGNIFICANT INTERCEPT TABLE

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
CPV_AN_DDH001	6.82	7.82	1	0.216	4.8
CPV_AN_DDH001	8.64	9.2	0.56	0.586	16.6
CPV_AN_DDH001	9.2	9.9	0.7	0.503	18.1
CPV_AN_DDH001	11	12	1	0.251	6.8
CPV_AN_DDH001	14	14.5	0.5	0.331	13.4
CPV_AN_DDH001	22.24	23	0.76	0.422	11.8
CPV_AN_DDH001	23	23.8	0.8	0.261	7.1
CPV_AN_DDH002	12.69	14	1.31	0.283	1.1
CPV_AN_DDH003	1.3	2.87	1.57	1.715	1.8
CPV_AN_DDH003	2.87	4	1.13	0.454	1.2
CPV_AN_DDH003	5	6	1	0.364	1.9
CPV_AN_DDH003	6	7.37	1.37	0.334	2.3
CPV_AN_DDH003	8.8	10	1.2	0.246	1
CPV_AN_DDH003	13	14	1	0.264	0.25
CPV_AN_DDH003	15	16	1	0.481	0.25
CPV_AN_DDH003	16	16.85	0.85	0.473	0.5
CPV_AN_DDH003	16.85	18	1.15	0.344	0.25
CPV_AN_DDH003	18	19	1	0.999	1.2
CPV_AN_DDH003	19	20	1	0.38	0.25

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
CPV_AN_DDH003	21	22	1	0.21	0.25
CPV_AN_DDH003	22.77	23.63	0.86	0.291	0.25
CPV_AN_DDH003	26	27	1	0.255	0.5
CPV_AN_DDH003	30.21	31	0.79	0.392	0.25
CPV_AN_DDH003	31	32	1	0.486	0.25
CPV_AN_DDH003	32	33	1	0.502	0.8
CPV_AN_DDH003	33	34	1	0.458	1.1
CPV_AN_DDH003	34	35.38	1.38	0.215	0.25
CPV_AN_DDH003	35.38	36	0.62	0.661	0.6
CPV_AN_DDH003	36	37	1	0.301	0.25
CPV_AN_DDH003	38	39	1	0.758	0.7
CPV_AN_DDH003	39	40	1	0.821	1.4
CPV_AN_DDH003	40	41	1	0.581	1
CPV_AN_DDH003	41	42	1	0.404	0.9
CPV_AN_DDH003	47	48	1	0.26	0.5
CPV_AN_DDH003	50	51	1	0.508	0.8
CPV_AN_DDH003	53.92	55	1.08	0.215	0.6
CPV_AN_DDH003	55	56	1	0.343	0.7
CPV_AN_DDH003	65	65.89	0.89	0.249	0.6
CPV_AN_DDH003	67	68	1	0.667	1.8
CPV_AN_DDH003	68	69.45	1.45	0.885	2.3
CPV_AN_DDH003	71	72	1	0.31	1.2
CPV_AN_DDH003	74.07	75	0.93	0.25	0.9
CPV_AN_DDH003	75	76	1	0.223	0.6
CPV_AN_DDH003	83	84	1	0.24	0.9
CPV_AN_DDH003	84	85	1	0.297	1.2
CPV_AN_DDH003	85	86	1	0.266	0.9
CPV_AN_DDH003	95	96	1	0.286	2.1
CPV_AN_DDH003	96	97.13	1.13	0.294	2.1
CPV_AN_DDH003	98	99	1	0.6	5.2
CPV_AN_DDH003	101	102.03	1.03	0.23	2.9
CPV_AN_DDH003	125	126.11	1.11	0.225	3.3
CPV_AN_DDH003	126.11	127	0.89	0.544	8.7
CPV_AN_DDH003	127	128	1	0.439	6.7
CPV_AN_DDH003	128	129	1	0.266	4.6
CPV_AN_DDH003	129	130	1	0.32	6.2
CPV_AN_DDH003	130	130.75	0.75	0.249	6
CPV_AN_DDH004	45	46.45	1.45	0.205	4.1
CPV_AN_DDH004	46.45	47	0.55	0.84	9.5
CPV_AN_DDH004	47	48	1	0.331	2
CPV_AN_DDH004	48	48.63	0.63	1.465	6.3
CPV_AN_DDH004	48.63	50	1.37	1.72	8.2
CPV_AN_DDH004	58	58.62	0.62	0.221	0.9
CPV_AN_DDH004	58.62	60	1.38	1.285	3.8
CPV_AN_DDH004	60	61	1	5.56	18
CPV_AN_DDH004	61	62	1	1.52	5
CPV_AN_DDH004	62	62.71	0.71	0.946	3.6
CPV_AN_DDH004	62.71	63.5	0.79	0.256	0.6
CPV_AN_DDH004	69	70	1	0.259	2.6
CPV_AN_DDH004	78	79	1	0.566	5.6
CPV_AN_DDH004	79	80	1	0.562	4.1
CPV_AN_DDH004	89	90	1	0.227	1.6
CPV_AN_DDH004	90	91	1	0.365	2.7
CPV_AN_DDH004	91	92	1	0.259	2.2
CPV_AN_DDH004	106	107	1	0.459	3.9
CPV_AN_DDH004	107	108	1	0.232	2.5

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
CPV_AN_DDH005	19.45	20	0.55	0.634	1.2
CPV_AN_DDH005	21	22	1	0.245	0.8
CPV_AN_DDH005	25	26	1	0.874	13.5
CPV_AN_DDH005	26	27	1	0.21	4.3
CPV_AN_DDH005	27	28	1	0.208	12.2
CPV_AN_DDH005	29	30	1	0.451	5.8
CPV_AN_DDH005	30	31	1	0.377	4.6
CPV_AN_DDH005	32	32.78	0.78	0.449	3.8
CPV_AN_DDH005	35.86	36.76	0.9	0.24	6.5
CPV_AN_DDH005	40	41	1	0.285	0.7
CPV_AN_DDH005	49	50	1	0.326	0.25
CPV_AN_DDH005	50	51	1	0.846	2
CPV_AN_DDH005	51	52	1	0.941	1.8
CPV_AN_DDH005	52	53	1	0.611	1.2
CPV_AN_DDH005	53	54	1	0.564	0.8
CPV_AN_DDH005	54	55	1	0.737	1
CPV_AN_DDH005	55	56	1	0.406	0.7
CPV_AN_DDH005	56	57	1	0.403	0.5
CPV_AN_DDH005	57	58	1	0.507	0.8
CPV_AN_DDH005	58	59	1	0.661	1.1
CPV_AN_DDH005	59	60	1	0.55	0.8
CPV_AN_DDH005	60	61	1	0.694	1.5
CPV_AN_DDH005	61	61.6	0.6	0.53	1.2
CPV_AN_DDH005	61.6	63	1.4	0.514	0.6
CPV_AN_DDH005	63	64	1	0.218	0.25
CPV_AN_DDH005	64	65	1	0.422	0.25
CPV_AN_DDH005	65	66	1	0.762	1.6
CPV_AN_DDH005	66	67	1	0.202	0.25
CPV_AN_DDH005	67	68	1	0.405	0.7
CPV_AN_DDH005	69	70	1	0.541	1.6
CPV_AN_DDH005	70	71	1	0.302	0.25
CPV_AN_DDH005	73	74	1	0.226	0.25
CPV_AN_DDH005	74	75	1	0.502	0.9
CPV_AN_DDH005	78	79	1	0.667	1.1
CPV_AN_DDH005	79	79.6	0.6	1.455	2.6
CPV_AN_DDH005	79.6	81	1.4	0.372	0.5
CPV_AN_DDH005	81	82	1	0.442	0.6
CPV_AN_DDH005	82	83	1	0.429	0.6
CPV_AN_DDH005	83	84	1	0.457	0.9
CPV_AN_DDH005	87	88.27	1.27	0.476	0.6
CPV_AN_DDH005	88.27	89	0.73	1.3	2.5
CPV_AN_DDH005	89	90	1	0.441	0.5
CPV_AN_DDH005	90	91	1	0.581	0.6
CPV_AN_DDH005	91	92	1	0.586	0.7
CPV_AN_DDH005	94	95	1	1.1	1.5
CPV_AN_DDH005	95	96	1	0.524	0.6
CPV_AN_DDH005	96	97	1	0.796	0.9
CPV_AN_DDH005	97	98	1	0.359	0.25
CPV_AN_DDH005	98	99	1	0.226	0.25
CPV_AN_DDH005	99	100	1	0.502	0.8
CPV_AN_DDH005	100	101	1	0.695	1.3
CPV_AN_DDH005	103	104	1	0.402	1.3
CPV_AN_DDH005	104.77	106	1.23	0.213	0.25
CPV_AN_DDH005	107	108	1	0.57	0.8
CPV_AN_DDH005	108	109	1	0.582	1
CPV_AN_DDH005	110.09	111	0.91	0.637	1

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
CPV_AN_DDH005	111	112	1	0.702	1.1
CPV_AN_DDH005	112	112.57	0.57	1.22	3.3
CPV_AN_DDH005	112.57	114	1.43	0.205	0.6
CPV_AN_DDH005	120	121	1	0.321	0.8
CPV_AN_DDH005	126	127	1	0.331	0.25
CPV_AN_DDH005	127	127.62	0.62	0.467	0.9
CPV_AN_DDH005	127.62	128.84	1.22	0.372	0.7
CPV_AN_DDH005	128.84	130	1.16	0.24	0.25
CPV_AN_DDH005	130	131	1	0.6	1.4
CPV_AN_DDH005	131	132	1	0.533	2
CPV_AN_DDH005	133	134	1	0.392	1
CPV_AN_DDH005	134	135	1	1.16	4.3
CPV_AN_DDH005	135	136	1	0.505	2.3
CPV_AN_DDH005	137	138	1	0.242	1
CPV_AN_DDH005	141	142	1	0.338	0.8
CPV_AN_DDH005	142	143	1	0.482	1
CPV_AN_DDH005	143	144	1	0.433	1.4
CPV_AN_DDH005	144	144.55	0.55	0.461	1.8
CPV_AN_DDH005	144.55	146	1.45	1.395	10.3
CPV_AN_DDH005	146	147	1	0.445	2.9
CPV_AN_DDH005	147	148	1	0.376	1.8
CPV_AN_DDH005	161	162	1	0.483	1.4
CPV_AN_DDH005	166	167	1	0.439	4.2
CPV_AN_DDH005	167	168	1	0.992	9.1
CPV_AN_DDH005	168	169	1	0.424	6.4
CPV_AN_DDH006	5.77	7	1.23	0.497	3.4
CPV_AN_DDH006	8	9	1	0.276	3.3
CPV_AN_DDH006	9	10	1	1.14	2.6
CPV_AN_DDH006	10	11	1	0.45	1
CPV_AN_DDH006	11	12	1	0.356	0.7
CPV_AN_DDH006	12	13	1	0.422	0.25
CPV_AN_DDH006	13	14	1	0.246	0.25
CPV_AN_DDH006	15	16	1	0.209	0.7
CPV_AN_DDH006	16	17	1	0.775	2.3
CPV_AN_DDH006	17	18	1	0.352	1
CPV_AN_DDH006	18	18.66	0.66	0.225	0.8
CPV_AN_DDH006	20.57	22	1.43	0.314	1.6
CPV_AN_DDH006	22	22.67	0.67	0.484	2.1
CPV_AN_DDH006	31	32.2	1.2	0.333	2.5
CPV_AN_DDH006	32.2	32.76	0.56	0.431	3.3
CPV_AN_DDH006	32.76	34	1.24	0.374	3.2
CPV_AN_DDH006	37	38	1	0.527	3.5
CPV_AN_DDH006	38	39	1	0.425	2.8
CPV_AN_DDH006	40.09	40.74	0.65	0.22	2.6
CPV_AN_DDH006	44	45	1	0.281	4.8
CPV_AN_DDH006	45	46	1	1.36	17.8
CPV_AN_DDH006	48	49	1	0.536	2.9
CPV_AN_DDH006	49	50	1	0.273	3.7
CPV_AN_DDH006	52	53	1	0.273	3.5
CPV_AN_DDH006	57	58	1	0.255	4.4
CPV_AN_DDH006	77	78	1	0.423	8.9
CPV_AN_DDH006	79	80	1	0.256	5.6
CPV_AN_DDH006	80	81	1	0.287	7.1
CPV_AN_DDH007	13	14	1	0.223	0.25
CPV_AN_DDH007	14	14.57	0.57	0.398	0.25
CPV_AN_DDH007	14.57	16	1.43	0.763	0.9

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
CPV_AN_DDH007	16	17.48	1.48	1.22	1.3
CPV_AN_DDH007	17.48	19	1.52	0.618	0.7
CPV_AN_DDH007	19	19.85	0.85	0.948	2.1
CPV_AN_DDH007	21	22	1	0.331	2.7
CPV_AN_DDH007	33	34	1	0.213	1.6
CPV_AN_DDH007	38.21	39	0.79	0.415	1.6
CPV_AN_DDH007	39	40	1	0.234	0.5
CPV_AN_DDH007	40	41	1	0.213	0.25
CPV_AN_DDH007	41	42.27	1.27	0.286	0.25
CPV_AN_DDH007	42.27	43	0.73	1.125	1.1
CPV_AN_DDH007	43	44	1	0.328	0.25
CPV_AN_DDH007	44	45	1	0.687	0.6
CPV_AN_DDH007	45	46	1	0.735	0.8
CPV_AN_DDH007	46	47	1	0.717	0.7
CPV_AN_DDH007	47	48	1	0.664	0.8
CPV_AN_DDH007	48	49	1	0.581	0.5
CPV_AN_DDH007	49	50	1	0.508	0.5
CPV_AN_DDH007	51	52.22	1.22	0.318	0.6
CPV_AN_DDH007	52.22	52.72	0.5	1.545	2.6
CPV_AN_DDH007	52.72	53.22	0.5	2.65	6
CPV_AN_DDH007	53.22	54.3	1.08	0.477	1
CPV_AN_DDH007	54.3	55	0.7	0.652	1.3
CPV_AN_DDH007	58	59	1	0.243	0.25
CPV_AN_DDH007	61	62	1	0.307	0.25
CPV_AN_DDH007	62	63.22	1.22	0.456	0.8
CPV_AN_DDH007	63.22	64	0.78	0.921	1.8
CPV_AN_DDH007	64	65	1	0.247	0.25
CPV_AN_DDH007	65	65.89	0.89	0.515	0.8
CPV_AN_DDH007	70	71	1	0.225	0.7
CPV_AN_DDH007	71	72	1	0.612	1.7
CPV_AN_DDH007	72	73	1	0.327	0.9
CPV_AN_DDH007	73	74	1	0.246	0.5
CPV_AN_DDH007	79.57	81	1.43	0.238	0.6
CPV_AN_DDH007	87	88	1	0.287	0.8
CPV_AN_DDH007	89	90	1	0.463	1.3
CPV_AN_DDH007	90	91	1	0.245	0.8
CPV_AN_DDH007	102	103	1	1.185	2.9
CPV_AN_DDH007	103	104	1	0.55	1.5
CPV_AN_DDH007	104	105	1	0.869	2.5
CPV_AN_DDH007	105	106	1	1.1	1.1
CPV_AN_DDH007	106	107	1	0.396	0.9
CPV_AN_DDH007	108.79	109.68	0.89	0.567	2
CPV_AN_DDH007	118.53	120	1.47	0.276	0.25
CPV_AN_DDH007	120	121	1	0.376	1.6
CPV_AN_DDH007	121	122	1	0.255	1.4
CPV_AN_DDH007	122	123	1	0.255	1.1
CPV_AN_DDH007	123	124	1	0.666	2
CPV_AN_DDH007	124	125	1	0.27	0.8
CPV_AN_DDH007	125	126	1	0.237	0.8
CPV_AN_DDH007	126	127.3	1.3	0.244	1
CPV_AN_DDH007	127.3	128	0.7	0.342	2.1
CPV_AN_DDH007	132	133	1	0.211	0.6
CPV_AN_DDH007	133	134	1	0.716	2.7
CPV_AN_DDH007	134	135	1	0.563	2.5
CPV_AN_DDH007	137	138	1	0.281	1.7
CPV_AN_DDH007	138.88	140	1.12	0.254	1

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
CPV_AN_DDH007	140	141	1	0.922	2.8
CPV_AN_DDH007	142	143	1	0.424	0.8
CPV_AN_DDH007	144.32	145	0.68	0.389	0.7
CPV_AN_DDH007	145	146	1	0.329	0.7
CPV_AN_DDH007	146	147	1	0.291	0.5
CPV_AN_DDH007	150	151	1	0.374	1
CPV_AN_DDH007	151	152	1	1.025	3.5
CPV_AN_DDH007	152	152.55	0.55	0.286	0.7
CPV_AN_DDH007	152.55	154	1.45	0.375	1
CPV_AN_DDH007	154	155.43	1.43	0.267	0.25
CPV_AN_DDH007	155.43	156	0.57	0.547	1.7
CPV_AN_DDH007	156	157	1	0.476	1.6
CPV_AN_DDH007	157	158	1	0.486	1.2
CPV_AN_DDH007	158	159	1	0.509	1.7
CPV_AN_DDH007	159	159.83	0.83	1.05	3.8
CPV_AN_DDH007	161	162	1	0.248	0.7
CPV_AN_DDH007	165	166	1	0.229	0.9
CPV_AN_DDH007	166	167	1	0.306	0.5
CPV_AN_DDH007	169	170	1	0.751	3
CPV_AN_DDH007	170	171	1	0.379	1.9
CPV_AN_DDH007	180	181	1	0.325	4.1
CPV_AN_DDH007	183	184	1	0.416	18.9
CPV_AN_DDH007	187	188	1	0.592	18.8
CPV_AN_DDH007	195	196	1	0.24	9.4
CPV_AN_DDH007	210	211	1	0.337	3.1
CPV_AN_DDH007	216	217	1	0.209	2.2
CPV_AN_DDH007	221	222	1	0.247	3.8
CPV_AN_DDH007	224	225	1	0.329	8.7
CPV_AN_DDH007	225	226	1	0.227	5.6
CPV_AN_DDH007	234	235	1	0.269	12.7
CPV_AN_DDH008	16	17	1	0.281	1.4
CPV_AN_DDH008	22	23	1	0.219	0.7
CPV_AN_DDH008	30.15	31	0.85	1.065	4.1
CPV_AN_DDH008	31	32	1	0.382	1.1
CPV_AN_DDH008	32	33	1	0.464	0.9
CPV_AN_DDH008	33	34	1	0.23	0.5
CPV_AN_DDH008	35	36	1	0.393	1.2
CPV_AN_DDH008	37	38	1	0.425	0.6
CPV_AN_DDH008	38	39	1	0.901	2
CPV_AN_DDH008	39	40	1	0.434	0.6
CPV_AN_DDH008	40	41	1	0.28	0.25
CPV_AN_DDH008	44	45	1	0.362	0.8
CPV_AN_DDH008	45	46	1	0.448	0.7
CPV_AN_DDH008	46	47	1	0.601	1
CPV_AN_DDH008	47	48	1	0.341	0.8
CPV_AN_DDH008	48	49	1	0.25	0.7
CPV_AN_DDH008	49	50.22	1.22	0.28	0.8
CPV_AN_DDH008	51.48	52	0.52	0.444	0.5
CPV_AN_DDH008	52	53	1	0.592	1
CPV_AN_DDH008	55	56	1	0.447	1.4
CPV_AN_DDH008	56	57	1	0.596	2.1
CPV_AN_DDH008	57	58	1	0.322	1
CPV_AN_DDH008	59	60.3	1.3	0.219	0.7
CPV_AN_DDH008	60.3	61	0.7	0.217	0.7
CPV_AN_DDH008	61	62	1	0.528	2.1
CPV_AN_DDH008	62	63	1	0.461	2.1

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
CPV_AN_DDH008	65	66	1	0.452	1.3
CPV_AN_DDH008	68	69	1	0.293	1
CPV_AN_DDH008	69	70	1	0.351	1
CPV_AN_DDH008	70	71	1	0.625	2.2
CPV_AN_DDH008	71	72	1	0.443	1.3
CPV_AN_DDH008	72	72.86	0.86	0.38	1.2
CPV_AN_DDH008	75	76	1	0.244	0.9
CPV_AN_DDH008	76	77	1	0.777	3
CPV_AN_DDH008	77	78	1	0.723	1.3
CPV_AN_DDH008	78	78.83	0.83	0.339	0.8
CPV_AN_DDH008	80	81	1	0.364	1.5
CPV_AN_DDH008	81	82	1	0.227	1.3
CPV_AN_DDH008	82	83.46	1.46	0.267	1.6
CPV_AN_DDH008	83.46	84	0.54	0.283	1.4
CPV_AN_DDH008	90.67	92	1.33	0.297	3
CPV_AN_DDH008	99	100	1	0.701	7.8
CPV_AN_DDH008	101	102	1	0.645	8
CPV_AN_DDH008	102	103	1	0.381	4.9
CPV_AN_DDH008	103	103.59	0.59	0.361	4.3
CPV_AN_DDH008	105	106	1	0.213	2.7
CPV_AN_DDH008	110	111	1	0.2	3.6
CPV_AN_DDH008	126	127	1	0.381	9.9
CPV_AN_DDH009	74.37	75	0.63	0.703	0.9
CPV_AN_DDH009	75	76	1	0.613	0.9
CPV_AN_DDH009	76	76.75	0.75	0.925	1.2
CPV_AN_DDH009	76.75	78	1.25	0.221	0.25
CPV_AN_DDH009	78	79	1	0.304	0.25
CPV_AN_DDH009	79	80	1	0.304	0.25
CPV_AN_DDH009	80	81	1	0.422	0.6
CPV_AN_DDH009	82	83	1	0.666	0.9
CPV_AN_DDH009	83	84	1	0.593	0.6
CPV_AN_DDH009	84	85	1	0.62	0.6
CPV_AN_DDH009	85	86	1	0.377	0.7
CPV_AN_DDH009	87	88	1	0.505	0.6
CPV_AN_DDH009	88	89	1	0.202	0.25
CPV_AN_DDH009	91	92	1	0.213	0.25
CPV_AN_DDH009	92	93	1	0.239	0.25
CPV_AN_DDH009	93	94.36	1.36	0.629	1.4
CPV_AN_DDH009	96	97	1	0.379	8.5
CPV_AN_DDH009	97	98	1	0.333	5.8
CPV_AN_DDH009	116	116.81	0.81	1.57	4.5
CPV_AN_DDH009	118	119	1	0.935	2.4
CPV_AN_DDH009	119	120	1	0.561	1.2
CPV_AN_DDH009	120	121	1	0.547	1.1
CPV_AN_DDH009	121	122	1	0.353	0.9
CPV_AN_DDH009	123	124	1	0.21	0.5
CPV_AN_DDH009	124	125	1	0.483	0.8
CPV_AN_DDH009	125	126	1	0.461	0.9
CPV_AN_DDH009	126	127	1	0.243	0.25
CPV_AN_DDH009	127	128	1	0.264	0.5
CPV_AN_DDH009	128	129	1	0.746	1.4
CPV_AN_DDH009	129	130	1	0.416	0.9
CPV_AN_DDH009	130	131	1	0.347	0.9
CPV_AN_DDH009	131	132	1	0.337	0.6
CPV_AN_DDH009	132	133	1	0.211	0.5
CPV_AN_DDH009	133	133.62	0.62	0.521	0.9

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
CPV_AN_DDH009	138	138.67	0.67	0.528	1.2
CPV_AN_DDH009	138.67	140	1.33	0.269	0.25
CPV_AN_DDH009	140	141	1	0.487	0.7
CPV_AN_DDH009	141	142	1	2.32	4.4
CPV_AN_DDH009	142	143	1	0.279	0.25
CPV_AN_DDH009	143	143.54	0.54	0.373	0.9
CPV_AN_DDH009	143.54	145	1.46	0.352	0.9
CPV_AN_DDH009	146	147.22	1.22	0.266	0.7
CPV_AN_DDH009	147.22	148	0.78	0.634	1.2
CPV_AN_DDH009	149.45	150	0.55	0.253	0.8
CPV_AN_DDH009	150	151	1	0.211	0.5
CPV_AN_DDH009	151	152	1	0.988	2
CPV_AN_DDH009	152	153	1	0.4	0.8
CPV_AN_DDH009	153	154.23	1.23	0.327	0.8
CPV_AN_DDH009	154.23	155	0.77	0.215	0.5
CPV_AN_DDH009	155	156	1	0.216	0.25
CPV_AN_DDH009	156	157	1	0.245	0.25
CPV_AN_DDH009	157	158	1	0.415	1.1
CPV_AN_DDH009	158	159	1	0.482	0.7
CPV_AN_DDH009	159	160	1	0.249	0.9
CPV_AN_DDH009	160	161	1	0.641	1
CPV_AN_DDH009	161	162	1	0.299	0.9
CPV_AN_DDH009	162	162.74	0.74	0.296	0.8
CPV_AN_DDH009	162.74	164	1.26	0.689	1.5
CPV_AN_DDH009	164	165	1	0.223	0.6
CPV_AN_DDH009	165	166	1	0.454	1
CPV_AN_DDH009	166	167	1	0.229	0.5
CPV_AN_DDH009	167	168	1	0.344	0.9
CPV_AN_DDH009	168	169	1	0.58	1.3
CPV_AN_DDH009	169	170	1	0.54	1.3
CPV_AN_DDH009	170	171	1	0.789	2
CPV_AN_DDH009	171	172	1	0.71	2.2
CPV_AN_DDH009	172	173	1	0.318	0.8
CPV_AN_DDH009	173	174	1	0.362	0.7
CPV_AN_DDH009	174	175	1	0.419	1.2
CPV_AN_DDH009	177	178	1	0.322	0.7
CPV_AN_DDH009	178	179	1	0.217	0.25
CPV_AN_DDH009	179	179.65	0.65	0.397	0.9
CPV_AN_DDH009	179.65	181	1.35	0.543	0.9
CPV_AN_DDH009	181	182	1	0.306	0.5
CPV_AN_DDH009	182	183	1	0.384	1
CPV_AN_DDH009	183	184	1	0.54	1.1
CPV_AN_DDH009	184	185	1	0.283	0.5
CPV_AN_DDH009	185	186	1	0.374	0.25
CPV_AN_DDH009	186	187	1	0.233	0.25
CPV_AN_DDH009	187	187.62	0.62	0.409	1.1
CPV_AN_DDH009	187.62	188.5	0.88	0.46	0.6
CPV_AN_DDH009	188.5	189.38	0.88	0.566	1.3
CPV_AN_DDH009	189.38	190	0.62	0.201	0.25
CPV_AN_DDH009	190	191	1	0.313	0.25
CPV_AN_DDH009	191	192	1	0.274	0.6
CPV_AN_DDH009	192	193	1	0.426	0.8
CPV_AN_DDH009	195	196	1	0.232	0.25
CPV_AN_DDH009	196	197	1	0.266	0.6
CPV_AN_DDH009	197	198	1	0.206	0.5
CPV_AN_DDH009	198	199	1	0.233	0.5

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
CPV_AN_DDH009	202.56	204	1.44	0.45	2.7
CPV_AN_DDH009	205	206	1	0.218	1.3
CPV_AN_DDH009	206	207.16	1.16	0.213	1.2
CPV_AN_DDH009	210.26	211	0.74	0.319	0.8
CPV_AN_DDH009	211	212	1	0.82	2.2
CPV_AN_DDH009	212	213	1	0.286	1.2
CPV_AN_DDH009	213	214	1	0.247	0.8
CPV_AN_DDH009	214	215.25	1.25	0.345	1
CPV_AN_DDH009	220	221	1	0.41	1.3
CPV_AN_DDH009	221	222	1	0.334	1
CPV_AN_DDH009	222	223	1	0.285	1
CPV_AN_DDH009	223	224	1	0.206	0.6
CPV_AN_DDH009	228.23	229	0.77	0.303	2.6
CPV_AN_DDH010	6	7	1	0.279	1.9
CPV_AN_DDH010	86	87	1	0.429	31.6
CPV_AN_DDH011	0	1	1	0.314	2
CPV_AN_DDH011	4	5	1	0.201	1.7
CPV_AN_DDH011	5	6	1	0.283	0.7
CPV_AN_DDH011	6	7	1	0.291	0.9
CPV_AN_DDH011	7	8	1	0.212	0.5
CPV_AN_DDH011	20.1	21.27	1.17	1.105	5
CPV_AN_DDH011	21.27	22	0.73	0.3	1.6
CPV_AN_DDH011	23	24	1	0.487	2.3
CPV_AN_DDH011	25	26	1	0.247	0.8
CPV_AN_DDH011	26	27	1	0.305	1
CPV_AN_DDH011	28	28.61	0.61	0.234	0.8
CPV_AN_DDH011	32	33	1	0.2	0.5
CPV_AN_DDH011	33	34.36	1.36	0.383	1.6
CPV_AN_DDH011	34.36	35	0.64	0.303	1.1
CPV_AN_DDH011	35	36	1	0.39	2.1
CPV_AN_DDH011	36	37	1	0.266	1.9
CPV_AN_DDH011	37	38	1	0.498	2.9
CPV_AN_DDH011	38	39	1	0.434	2.4
CPV_AN_DDH011	39	40	1	0.202	0.8
CPV_AN_DDH011	41	42	1	0.674	3.5
CPV_AN_DDH011	42	43	1	0.586	3.1
CPV_AN_DDH011	43	44	1	0.279	1.2
CPV_AN_DDH011	44	44.9	0.9	0.399	1.7
CPV_AN_DDH011	46	47	1	0.298	2
CPV_AN_DDH011	49	50	1	0.868	4.9
CPV_AN_DDH011	50	51	1	2.6	12.5
CPV_AN_DDH012	62.35	63	0.65	0.513	2.2
CPV_AN_DDH012	63	64	1	0.891	3.5
CPV_AN_DDH012	64	65	1	0.556	2.2
CPV_AN_DDH012	65	66	1	0.714	2.8
CPV_AN_DDH012	66	67.19	1.19	0.521	2.2
CPV_AN_DDH012	72	73	1	0.263	1
CPV_AN_DDH012	76	77	1	0.233	1.1
CPV_AN_DDH012	82	83	1	0.316	0.5
CPV_AN_DDH012	83	84	1	0.244	0.25
CPV_AN_DDH012	84	85	1	0.222	0.25
CPV_AN_DDH012	85	86	1	0.259	0.9
CPV_AN_DDH012	86	87	1	0.237	2.4
CPV_AN_DDH012	120.52	122	1.48	0.259	1.4
CPV_AN_DDH012	122	123	1	0.729	2.5
CPV_AN_DDH012	123	124	1	0.366	0.8

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
CPV_AN_DDH012	124	125.15	1.15	0.682	3.8
CPV_AN_DDH012	142.6	143.97	1.37	0.266	1.1
CPV_AN_DDH012	145.91	147	1.09	0.492	1.5
CPV_AN_DDH012	147	148	1	0.488	1.1
CPV_AN_DDH012	148	149	1	0.555	1
CPV_AN_DDH012	149	150	1	0.401	1.3
CPV_AN_DDH012	152	153	1	0.471	0.8
CPV_AN_DDH012	153	154	1	0.54	1.1
CPV_AN_DDH012	154	155	1	0.376	1.2
CPV_AN_DDH012	155	155.94	0.94	0.225	0.7
CPV_AN_DDH012	155.94	157.08	1.14	0.408	2.1
CPV_AN_DDH012	158	159	1	0.441	2.3
CPV_AN_DDH012	169.68	171	1.32	0.238	1.8
CPV_AN_DDH012	171	172	1	0.342	1.8
CPV_AN_DDH012	177	178	1	0.223	3.7
CPV_AN_DDH013	39.24	40	0.76	0.291	1.3
CPV_AN_DDH013	40	41	1	0.618	1.5
CPV_AN_DDH013	41	42	1	0.272	3.9
CPV_AN_DDH013	114.47	115.89	1.42	0.264	0.5
CPV_AN_DDH014	102.05	103	0.95	0.28	7.8
CPV_AN_DDH014	103	104	1	0.326	2.3
CPV_AN_DDH014	104	105	1	0.209	2.6
CPV_AN_DDH014	106	107	1	0.202	1.2
CPV_AN_DDH014	107	108	1	0.234	1.8
CPV_AN_DDH014	163	164	1	0.322	7.8
CPV_AN_DDH014	164	165	1	0.323	6.6
CPV_AN_DDH014	166	167	1	1.065	25.7
CPV_AN_DDH014	178	179	1	0.475	10.3
CPV_AN_DDH014	179	179.7	0.7	0.664	16.2
CPV_AN_DDH014	179.7	180.5	0.8	0.237	4.9
CPV_AN_DDH014	181.28	182	0.72	0.974	23.6
CPV_AN_DDH014	184	185	1	0.343	5.6
CPV_AN_DDH014	186	187	1	0.817	15.3
CPV_AN_DDH014	187	188	1	0.476	9.1
CPV_AN_DDH014	189.95	191	1.05	0.762	17.4
CPV_AN_DDH014	191	192	1	1.445	26.7
CPV_AN_DDH015	20.39	21	0.61	0.334	1
CPV_AN_DDH015	21	22	1	0.236	0.25
CPV_AN_DDH015	22	23	1	0.279	1
CPV_AN_DDH015	23	24	1	0.286	2
CPV_AN_DDH015	24.59	26	1.41	0.43	2
CPV_AN_DDH015	33	34	1	0.222	0.25
CPV_AN_DDH015	34	34.88	0.88	0.595	1
CPV_AN_DDH015	34.88	36	1.12	0.24	0.25
CPV_AN_DDH015	45	46	1	0.267	2
CPV_AN_DDH015	47	48	1	0.213	1
CPV_AN_DDH015	48	49	1	0.524	3
CPV_AN_DDH015	49	50	1	0.571	2
CPV_AN_DDH015	50	51	1	0.62	4
CPV_AN_DDH015	51	52	1	0.271	0.25
CPV_AN_DDH015	52	53	1	0.786	3
CPV_AN_DDH015	53	54	1	0.439	1
CPV_AN_DDH015	54	55	1	0.494	2
CPV_AN_DDH015	56	57	1	0.369	1
CPV_AN_DDH015	58	59	1	0.452	1
CPV_AN_DDH015	59	60	1	0.216	0.25

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
CPV_AN_DDH015	62	63	1	0.228	1
CPV_AN_DDH015	74	75	1	0.239	1
CPV_AN_DDH015	76	77	1	0.236	1
CPV_AN_DDH015	77	78.13	1.13	0.235	0.25
CPV_AN_DDH015	92	93	1	0.223	0.25
CPV_AN_DDH015	93	94	1	0.209	1
CPV_AN_DDH015	124	125	1	0.319	1
CPV_AN_DDH015	125	126.04	1.04	0.666	5
CPV_AN_DDH015	126.04	126.7	0.66	0.651	5
CPV_AN_DDH015	126.7	128	1.3	0.252	2
CPV_AN_DDH015	130	131	1	0.207	4
CPV_AN_DDH015	140	141	1	0.202	4
CPV_AN_DDH016	1.05	2	0.95	1.6	5
CPV_AN_DDH016	2	3	1	1.58	4
CPV_AN_DDH016	3	3.67	0.67	3.89	27
CPV_AN_DDH016	4.5	5.39	0.89	0.268	7
PRI_AN_DDH020	60	61	1	0.4	2
PRI_AN_DDH027	196.78	198	1.22	1.28	3
PRI_AN_DDH027	198	199.5	1.5	1.14	2
PRI_AN_DDH027	199.5	200	0.5	0.916	1
PRI_AN_DDH027	200	201	1	0.816	2
PRI_AN_DDH027	201	202	1	0.865	1
PRI_AN_DDH027	202	203	1	0.556	0.25
PRI_AN_DDH027	203	204	1	0.479	0.25
PRI_AN_DDH027	204	205	1	0.731	1
PRI_AN_DDH027	205	206	1	0.354	1
PRI_AN_DDH027	206	207	1	0.222	1
PRI_AN_DDH027	208.17	209	0.83	0.568	3
PRI_AN_DDH027	212.52	214	1.48	0.254	0.25
PRI_AN_DDH027	219.3	220	0.7	0.259	2
PRI_AN_DDH027	222	223	1	0.44	3
PRI_AN_DDH027	223	224	1	0.223	3
PRI_AN_DDH027	228	229	1	0.206	5
PRI_AN_DDH027	229	230	1	0.441	15
PRI_AN_DDH027	241	242	1	0.247	1
PRI_AN_DDH027	242	243	1	0.308	0.25
PRI_AN_DDH027	243	244	1	0.601	20
PRI_AN_DDH027	244	245	1	0.315	12
PRI_AN_DDH027	245	246	1	0.212	10
PRI_AN_DDH027	250	251	1	0.264	2
PRI_AN_DDH027	255	256	1	0.221	6
PRI_AN_DDH027	263	264	1	0.27	3
PRI_AN_DDH027	264	265	1	0.928	7
PRI_AN_DDH027	266.35	267	0.65	0.256	2
PRI_AN_DDH027	270	271	1	0.24	1
PRI_AN_DDH027	271	271.94	0.94	0.231	1
PRI_AN_DDH027	273	274	1	0.359	3
PRI_AN_DDH027	274	275	1	0.368	4
PRI_AN_DDH027	275	276	1	0.514	5
PRI_AN_DDH027	276	277	1	0.392	0.25
PRI_AN_DDH027	277	278	1	0.408	1
PRI_AN_DDH027	278	279	1	0.315	0.25
PRI_AN_DDH027	279	280	1	0.333	0.25
PRI_AN_DDH027	281	282	1	0.354	4
PRI_AN_DDH027	284	285	1	0.359	4
PRI_AN_DDH027	285	286	1	0.233	2

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
PRI_AN_DDH027	286	287	1	0.32	2
PRI_AN_DDH027	288	289	1	0.483	1
PRI_AN_DDH027	289	290	1	0.223	0.25
PRI_AN_DDH027	290	291	1	0.215	0.25
PRI_AN_DDH027	291	292	1	0.313	1
PRI_AN_DDH027	292.64	294	1.36	0.207	0.25
PRI_AN_DDH027	296	297	1	0.249	1
PRI_AN_DDH027	297	298	1	0.2	0.25
PRI_AN_DDH027	298	299	1	0.293	1
PRI_AN_DDH027	299	300	1	0.265	0.25
PRI_AN_DDH027	303	303.72	0.72	1.035	2
PRI_AN_DDH027	303.72	305	1.28	0.36	1
PRI_AN_DDH027	305	306	1	0.296	0.25
PRI_AN_DDH027	308	309	1	0.307	0.25
PRI_AN_DDH027	312	313	1	0.262	1
PRI_AN_DDH027	313	314	1	0.499	2
PRI_AN_DDH027	315	316	1	0.322	2
PRI_AN_DDH027	316	317	1	0.452	1
PRI_AN_DDH027	320	321	1	0.331	1
PRI_AN_DDH027	323	323.87	0.87	0.283	2
PRI_AN_DDH027	324.95	326	1.05	0.292	0.25
PRI_AN_DDH027	326	327	1	0.233	0.25
PRI_AN_DDH027	331	332	1	0.219	2
PRI_AN_DDH027	332	333	1	0.338	1
PRI_AN_DDH027	333	334.26	1.26	0.571	2
PRI_AN_DDH027	339	340	1	0.248	0.25
PRI_AN_DDH027	344.45	345	0.55	0.29	1
PRI_AN_DDH027	345	346	1	0.769	4
PRI_AN_DDH027	346	346.78	0.78	0.211	1
PRI_AN_DDH027	346.78	347.5	0.72	1.335	5
PRI_AN_DDH027	348.43	349.66	1.23	0.428	2
PRI_AN_DDH027	353	354	1	0.703	5
PRI_AN_DDH027	354	355	1	0.63	5
PRI_AN_DDH027	359	360	1	0.299	3
PRI_AN_DDH027	361	362	1	0.403	3
PRI_AN_DDH027	363	364	1	0.308	2
PRI_AN_DDH027	365	366	1	0.521	5
PRI_AN_DDH027	366	367	1	0.278	2
PRI_AN_DDH027	368	369	1	0.486	2
PRI_AN_DDH027	369	370.07	1.07	0.269	3
PRI_AN_DDH027	370.07	370.68	0.61	1.88	8
PRI_AN_DDH027	378.9	380	1.1	1.695	13
PRI_AN_DDH027	391	392	1	0.347	2
PRI_AN_DDH027	401	402	1	0.363	3
PRI_AN_DDH027	409	410	1	0.505	3
PRI_AN_DDH027	413	414	1	0.518	3
PRI_AN_DDH027	415	416.1	1.1	0.432	5
PRI_AN_DDH028	6.74	8	1.26	0.988	2
PRI_AN_DDH028	8	9	1	0.481	1
PRI_AN_DDH028	9	10	1	0.469	1
PRI_AN_DDH028	10	11	1	0.4	2
PRI_AN_DDH028	11	12	1	0.449	3
PRI_AN_DDH028	12	13	1	0.405	3
PRI_AN_DDH028	13	14	1	0.411	3
PRI_AN_DDH028	14	15	1	0.379	3
PRI_AN_DDH028	15	16	1	0.258	1

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
PRI_AN_DDH028	16	17	1	0.512	18
PRI_AN_DDH028	17	18	1	0.41	63
PRI_AN_DDH028	18	19	1	0.735	24
PRI_AN_DDH028	19	19.65	0.65	0.777	13
PRI_AN_DDH029	74.84	76	1.16	0.362	0.25
PRI_AN_DDH029	76	76.74	0.74	0.482	3
PRI_AN_DDH029	76.74	78	1.26	0.707	4
PRI_AN_DDH029	78	78.75	0.75	0.721	3
PRI_AN_DDH029	78.75	80.03	1.28	0.241	2
PRI_AN_DDH029	87	88	1	0.208	1
PRI_AN_DDH029	94	95	1	0.217	6
PRI_AN_DDH029	199	200	1	0.486	20
PRI_AN_DDH030	60.55	62	1.45	0.866	2
PRI_AN_DDH030	62	63	1	3.17	12
PRI_AN_DDH030	63	64	1	2.41	4
PRI_AN_DDH030	64	65	1	1.77	4
PRI_AN_DDH030	65	66	1	1.49	2
PRI_AN_DDH030	66	67.19	1.19	2.23	3
PRI_AN_DDH030	67.19	67.8	0.61	2.01	3
PRI_AN_DDH030	67.8	69	1.2	6.09	6
PRI_AN_DDH030	69	70	1	2.39	1
PRI_AN_DDH030	70	71	1	1.005	0.25
PRI_AN_DDH030	71	72	1	2.17	1
PRI_AN_DDH030	72	73	1	1.655	0.25
PRI_AN_DDH030	73	74	1	2.02	0.25
PRI_AN_DDH030	74	75	1	0.901	0.25
PRI_AN_DDH030	75	76	1	4.92	6
PRI_AN_DDH030	76	77	1	3.27	3
PRI_AN_DDH030	77	78	1	1.88	3
PRI_AN_DDH030	78	79	1	0.953	2
PRI_AN_DDH030	79	80	1	0.391	1
PRI_AN_DDH030	80	80.5	0.5	1.18	1
PRI_AN_DDH030	80.5	82	1.5	3.82	8
PRI_AN_DDH030	82	83.39	1.39	0.421	2
PRI_AN_DDH030	85	86	1	0.497	0.25
PRI_AN_DDH030	87	88	1	0.777	7
PRI_AN_DDH030	88	89.1	1.1	0.992	10
PRI_AN_DDH030	89.1	90	0.9	0.582	8
PRI_AN_DDH031	105	106	1	0.714	9
PRI_AN_DDH031	112.15	112.8	0.65	0.286	3
PRI_AN_DDH033	215.02	216	0.98	0.214	0.25
PRI_AN_DDH033	216	217.08	1.08	0.255	2
PRI_AN_DDH033	217.08	218	0.92	0.267	2
PRI_AN_DDH033	219	220	1	0.4	5
PRI_AN_DDH033	220	221.49	1.49	0.442	3
PRI_AN_DDH033	224	225	1	0.394	4
PRI_AN_DDH033	230	231	1	0.644	10
PRI_AN_DDH033	232	233	1	0.245	5
PRI_AN_DDH033	241.47	242.74	1.27	0.211	5
PRI_AN_DDH033	242.74	244	1.26	0.476	11
PRI_AN_DDH033	244	245	1	0.389	7
PRI_AN_DDH033	260	261	1	0.357	3
PRI_AN_DDH033	261	262	1	0.251	1
PRI_AN_DDH033	262	263	1	0.207	1
PRI_AN_DDH033	263.97	264.68	0.71	0.293	4
PRI_AN_DDH033	264.68	266	1.32	0.229	5

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
PRI_AN_DDH033	274.5	275.46	0.96	0.308	2
PRI_AN_DDH033	281	282.39	1.39	0.214	0.25
PRI_AN_DDH033	292.17	292.88	0.71	0.36	3
PRI_AN_DDH033	293.63	295	1.37	0.701	9
PRI_AN_DDH033	295	296	1	0.286	1
PRI_AN_DDH033	296	296.69	0.69	0.516	2
PRI_AN_DDH033	298	299	1	0.268	1
PRI_AN_DDH033	299	300.11	1.11	0.368	6
PRI_AN_DDH033	300.11	301	0.89	0.552	8
PRI_AN_DDH033	301	302	1	0.452	8
PRI_AN_DDH033	302	302.95	0.95	0.474	6
PRI_AN_DDH033	302.95	304	1.05	0.559	6
PRI_AN_DDH033	304	305	1	0.322	3
PRI_AN_DDH033	305	306	1	0.25	1
PRI_AN_DDH033	306	307	1	0.307	1
PRI_AN_DDH033	307	307.72	0.72	0.219	0.25
PRI_AN_DDH033	309	310	1	0.327	1
PRI_AN_DDH033	310	311.36	1.36	0.301	2
PRI_AN_DDH033	320	321	1	0.341	1
PRI_AN_DDH033	322	322.93	0.93	0.245	1
PRI_AN_DDH033	322.93	323.98	1.05	0.691	4
PRI_AN_DDH033	325	326.12	1.12	0.261	3
PRI_AN_DDH033	326.12	327	0.88	0.456	1
PRI_AN_DDH033	327	328	1	0.293	1
PRI_AN_DDH033	335	336	1	0.358	1
PRI_AN_DDH033	336	337.05	1.05	0.242	1
PRI_AN_DDH033	342	343	1	0.604	2
PRI_AN_DDH033	343	344	1	0.279	0.25
PRI_AN_DDH033	344	345	1	0.673	2
PRI_AN_DDH033	345	346	1	0.353	2
PRI_AN_DDH033	347	348	1	0.218	0.25
PRI_AN_DDH033	349.2	349.73	0.53	0.254	0.25
PRI_AN_DDH033	349.73	350.5	0.77	0.717	1
PRI_AN_DDH033	350.5	351.4	0.9	0.512	1
PRI_AN_DDH033	352	353	1	0.53	1
PRI_AN_DDH033	353	354	1	0.23	0.25
PRI_AN_DDH033	358	359.41	1.41	0.435	1
PRI_AN_DDH033	359.41	360	0.59	0.347	0.25
PRI_AN_DDH033	360	361	1	0.419	0.25
PRI_AN_DDH033	363.76	365	1.24	0.28	0.25
PRI_AN_DDH033	369.6	371	1.4	0.363	7
PRI_AN_DDH033	381	382	1	0.483	7
PRI_AN_DDH033	382	383	1	0.634	3
PRI_AN_DDH033	385	386	1	0.818	1
PRI_AN_DDH033	388	389	1	0.373	2
PRI_AN_DDH033	392	393	1	0.474	4
PRI_AN_DDH033	395	396.12	1.12	0.467	3
PRI_AN_DDH033	396.12	397	0.88	0.302	3
PRI_AN_DDH033	400	401	1	0.261	0.25
PRI_AN_DDH033	404	405	1	0.4	0.25
PRI_AN_DDH033	405	406	1	0.357	1
PRI_AN_DDH033	406	407	1	0.393	3
PRI_AN_DDH033	407	408	1	0.252	2
PRI_AN_DDH033	408	409	1	1.21	11
PRI_AN_DDH033	409	410	1	0.782	6
PRI_AN_DDH033	410	411	1	0.666	6

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
PRI_AN_DDH033	413	414	1	0.771	10
PRI_AN_DDH033	414	415	1	0.516	7
PRI_AN_DDH033	415	416	1	0.436	1
PRI_AN_DDH033	416	417	1	0.441	3
PRI_AN_DDH033	417	417.56	0.56	0.362	2
PRI_AN_DDH033	417.56	418.11	0.55	1.8	18
PRI_AN_DDH033	418.11	418.84	0.73	0.258	6
PRI_AN_DDH033	419.34	420.32	0.98	0.402	2
PRI_AN_DDH033	423	424.5	1.5	0.848	2
PRI_AN_DDH033	424.5	426	1.5	0.496	0.25
PRI_AN_DDH033	426	427	1	0.302	0.25
PRI_AN_DDH033	428	429	1	0.262	0.25
PRI_AN_DDH033	429	430	1	0.616	3
PRI_AN_DDH033	430	431	1	1.03	3
PRI_AN_DDH033	431	432	1	0.751	3
PRI_AN_DDH033	432	433	1	0.8	4
PRI_AN_DDH033	433	434	1	0.428	2
PRI_AN_DDH033	438	439	1	0.241	1
PRI_AN_DDH033	445.02	445.59	0.57	0.205	0.25
PRI_AN_DDH033	447.14	448	0.86	0.321	1
PRI_AN_DDH033	448	449	1	0.237	0.25
PRI_AN_DDH033	461	462	1	0.242	0.25
PRI_AN_DDH033	465.33	466	0.67	0.248	1
PRI_AN_DDH033	466	467	1	0.218	1
PRI_AN_DDH033	469	470	1	0.265	1
PRI_AN_DDH033	471	472	1	1.215	5
PRI_AN_DDH033	473	474	1	3.45	16
PRI_AN_DDH033	485	486.25	1.25	0.291	1
PRI_AN_DDH033	492	493	1	0.243	2
PRI_AN_DDH033	494	495	1	0.375	1
PRI_AN_DDH033	499	500	1	0.239	2
PRI_AN_DDH034	1	2	1	0.258	9
PRI_AN_DDH034	2	3	1	0.496	6
PRI_AN_DDH034	3	4	1	0.267	3
PRI_AN_DDH034	7	8	1	0.328	0.25
PRI_AN_DDH034	12	13	1	5.03	50
PRI_AN_DDH034	15	16	1	0.54	7
PRI_AN_DDH034	17.45	18.23	0.78	0.667	9
PRI_AN_DDH034	18.23	19	0.77	0.215	2
PRI_AN_DDH034	27	28	1	0.566	6
PRI_AN_DDH034	32	33.17	1.17	0.583	5
PRI_AN_DDH034	33.17	33.81	0.64	0.346	2
PRI_AN_DDH034	36.94	38	1.06	0.311	4
PRI_AN_DDH034	38	39	1	0.423	5
PRI_AN_DDH034	46	47	1	0.31	1
PRI_AN_DDH034	48	48.67	0.67	0.249	2
PRI_AN_DDH034	50	50.72	0.72	0.33	1
PRI_AN_DDH034	53	54	1	0.605	5
PRI_AN_DDH034	54	54.98	0.98	0.45	4
PRI_AN_DDH034	54.98	56.38	1.4	0.395	3
PRI_AN_DDH034	58	59	1	0.384	3
PRI_AN_DDH034	59	60	1	0.516	6
PRI_AN_DDH034	60	61	1	0.272	4
PRI_AN_DDH034	83	84	1	0.274	5
PRI_AN_DDH035	129.88	131	1.12	0.587	1
PRI_AN_DDH035	131	132	1	0.52	1

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
PRI_AN_DDH035	132	133	1	0.234	3
PRI_AN_DDH035	142.8	144	1.2	0.225	5
PRI_AN_DDH037	0	1	1	0.714	2
PRI_AN_DDH037	1	2	1	0.327	2
PRI_AN_DDH037	3	4	1	0.251	1
PRI_AN_DDH037	12	13	1	0.637	12
PRI_AN_DDH038	54	55	1	0.658	3
PRI_AN_DDH038	55	56	1	0.357	3
PRI_AN_DDH039	126.5	128	1.5	0.334	1
PRI_AN_DDH040	164.75	166	1.25	0.68	1
PRI_AN_DDH040	166	167	1	1.07	0.25
PRI_AN_DDH040	167	168	1	0.862	1
PRI_AN_DDH040	168	169	1	0.831	0.25
PRI_AN_DDH040	169	170.43	1.43	0.641	0.25
PRI_AN_DDH040	176.44	177	0.56	0.235	0.25
PRI_AN_DDH040	186.15	187	0.85	0.345	0.25
PRI_AN_DDH040	188.33	189.45	1.12	1.14	2
PRI_AN_DDH040	189.45	190.25	0.8	0.549	2
PRI_AN_DDH040	190.25	191	0.75	0.723	1
PRI_AN_DDH040	191	192	1	0.559	0.25
PRI_AN_DDH040	192	193	1	1.07	2
PRI_AN_DDH040	193	194.16	1.16	0.663	0.25
PRI_AN_DDH040	194.16	194.96	0.8	0.362	0.25
PRI_AN_DDH040	195.91	197	1.09	0.409	1
PRI_AN_DDH040	197	198	1	0.657	1
PRI_AN_DDH040	198	199	1	0.385	1
PRI_AN_DDH040	199	200	1	0.885	1
PRI_AN_DDH040	200	201	1	0.739	0.25
PRI_AN_DDH040	201	202.08	1.08	0.651	1
PRI_AN_DDH040	202.64	204	1.36	0.24	0.25
PRI_AN_DDH040	205	205.67	0.67	0.225	0.25
PRI_AN_DDH040	205.67	206.5	0.83	0.48	1
PRI_AN_DDH040	206.5	207.23	0.73	1.47	2
PRI_AN_DDH040	207.23	208	0.77	0.414	0.25
PRI_AN_DDH040	208	209	1	1.35	2
PRI_AN_DDH040	209	210	1	0.636	1
PRI_AN_DDH040	210.9	212	1.1	0.794	0.25
PRI_AN_DDH040	212	213	1	0.295	1
PRI_AN_DDH040	216.54	218	1.46	1.06	2
PRI_AN_DDH040	221.34	222.75	1.41	0.211	1
PRI_AN_DDH040	222.75	224	1.25	0.305	1
PRI_AN_DDH040	225	226	1	0.355	2
PRI_AN_DDH040	226	227	1	0.603	1
PRI_AN_DDH040	227	228	1	0.228	1
PRI_AN_DDH040	229.83	231	1.17	0.285	1
PRI_AN_DDH040	231	232	1	0.223	2
PRI_AN_DDH040	232.62	234	1.38	0.215	0.25
PRI_AN_DDH040	234	235	1	0.245	0.25
PRI_AN_DDH040	239.4	240	0.6	0.265	1
PRI_AN_DDH040	240	241	1	0.231	1
PRI_AN_DDH040	248	249	1	0.209	1
PRI_AN_DDH040	251	252	1	0.995	1
PRI_AN_DDH040	252	253	1	0.666	0.25
PRI_AN_DDH040	253	254	1	0.597	2
PRI_AN_DDH040	254	255	1	0.525	1
PRI_AN_DDH040	255	256	1	0.279	1

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
PRI_AN_DDH040	256	256.59	0.59	0.308	0.25
PRI_AN_DDH040	256.59	257.24	0.65	0.357	0.25
PRI_AN_DDH040	257.24	258.2	0.96	0.214	1
PRI_AN_DDH040	258.2	259.55	1.35	0.599	2
PRI_AN_DDH040	260.52	262	1.48	0.223	1
PRI_AN_DDH040	265	266.02	1.02	0.506	1
PRI_AN_DDH040	266.02	267	0.98	0.255	0.25
PRI_AN_DDH040	267	268	1	0.215	1
PRI_AN_DDH040	270	271	1	0.244	0.25
PRI_AN_DDH040	271	272	1	0.254	0.25
PRI_AN_DDH040	272	273	1	0.273	0.25
PRI_AN_DDH040	274	275.09	1.09	0.557	0.25
PRI_AN_DDH040	275.67	276.5	0.83	0.418	2
PRI_AN_DDH040	276.5	277.46	0.96	0.344	0.25
PRI_AN_DDH040	278	279	1	0.262	0.25
PRI_AN_DDH040	279	280	1	0.737	0.25
PRI_AN_DDH040	280	281.36	1.36	0.575	0.25
PRI_AN_DDH040	281.36	282	0.64	0.313	0.25
PRI_AN_DDH040	282	283	1	0.244	2
PRI_AN_DDH040	283	284	1	0.529	0.25
PRI_AN_DDH040	284	285	1	0.59	1
PRI_AN_DDH040	285	286	1	1.16	1
PRI_AN_DDH040	286	287.48	1.48	0.753	1
PRI_AN_DDH040	287.48	288.75	1.27	1.03	2
PRI_AN_DDH040	288.75	289.64	0.89	1.24	3
PRI_AN_DDH040	289.64	291	1.36	0.916	4
PRI_AN_DDH040	291	292.44	1.44	1.11	1
PRI_AN_DDH040	292.44	293	0.56	1.58	4
PRI_AN_DDH040	293	294	1	1.38	3
PRI_AN_DDH040	294	295	1	1.9	4
PRI_AN_DDH040	295	296.03	1.03	0.776	2
PRI_AN_DDH040	296.03	297	0.97	0.635	1
PRI_AN_DDH040	297	298	1	0.568	1
PRI_AN_DDH040	298	299	1	0.713	1
PRI_AN_DDH040	299	300	1	0.465	1
PRI_AN_DDH040	300	301	1	0.557	2
PRI_AN_DDH040	301	302	1	0.901	2
PRI_AN_DDH040	302	303	1	0.749	2
PRI_AN_DDH040	305	306	1	0.283	0.25
PRI_AN_DDH040	306	306.59	0.59	0.378	1
PRI_AN_DDH040	307.1	308	0.9	0.59	3
PRI_AN_DDH040	308	309.37	1.37	0.615	3
PRI_AN_DDH040	309.37	310.05	0.68	0.996	4
PRI_AN_DDH040	310.05	311	0.95	1.04	4
PRI_AN_DDH040	311	312	1	0.681	2
PRI_AN_DDH040	312	313	1	0.289	2
PRI_AN_DDH040	313	314	1	0.372	1
PRI_AN_DDH040	317.33	318	0.67	0.475	1
PRI_AN_DDH040	326	327	1	0.285	1
PRI_AN_DDH040	327	328.12	1.12	0.469	2
PRI_AN_DDH040	330.14	331	0.86	0.312	0.25
PRI_AN_DDH040	331	332	1	2.15	9
PRI_AN_DDH040	332	333.45	1.45	0.613	2
PRI_AN_DDH040	333.45	334	0.55	6.48	50
PRI_AN_DDH040	335	336	1	0.292	2
PRI_AN_DDH040	336	337	1	1.46	17

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
PRI_AN_DDH040	337	338	1	0.841	15
PRI_AN_DDH040	338	339	1	2.5	33
PRI_AN_DDH040	347	348	1	0.326	4
PRI_AN_DDH040	348	349	1	4.68	57
PRI_AN_DDH040	349	350	1	0.386	5
PRI_AN_DDH040	350	351	1	0.35	4
PRI_AN_DDH040	356.24	357	0.76	0.201	2
PRI_AN_DDH040	375	376	1	0.291	3
PRI_AN_DDH041	155.7	156.44	0.74	0.733	15
PRI_AN_DDH041	175.22	176.12	0.9	0.298	7
PRI_AN_DDH041	176.12	177.3	1.18	0.922	11
PRI_AN_DDH041	177.3	177.8	0.5	0.243	5
PRI_AN_DDH041	177.8	179	1.2	0.502	8
PRI_AN_DDH041	180	181.33	1.33	0.545	13
PRI_AN_DDH041	188.2	188.88	0.68	0.272	29
PRI_AN_DDH041	196.27	197	0.73	0.345	21
PRI_AN_DDH041	197	198	1	0.717	39
PRI_AN_DDH041	229	230	1	0.28	1
PRI_AN_DDH042	0	1	1	0.811	2
PRI_AN_DDH042	1	2	1	0.319	0.25
PRI_AN_DDH042	3	4	1	0.405	1
PRI_AN_DDH042	5.95	7	1.05	1.05	0.25
PRI_AN_DDH042	7	8.37	1.37	0.267	0.25
PRI_AN_DDH042	9.14	10	0.86	0.851	3
PRI_AN_DDH042	10	11	1	0.522	0.25
PRI_AN_DDH042	11	12	1	0.201	0.25
PRI_AN_DDH042	12	13.45	1.45	0.712	1
PRI_AN_DDH042	13.45	14	0.55	0.652	0.25
PRI_AN_DDH042	14	15	1	0.974	2
PRI_AN_DDH042	15	16	1	0.509	1
PRI_AN_DDH042	16	17	1	1.42	2
PRI_AN_DDH042	17	18	1	0.832	1
PRI_AN_DDH042	18	18.65	0.65	0.827	1
PRI_AN_DDH042	18.65	20.1	1.45	0.417	1
PRI_AN_DDH042	20.1	21	0.9	0.358	0.25
PRI_AN_DDH042	21	22	1	0.644	1
PRI_AN_DDH042	22	23	1	0.978	2
PRI_AN_DDH042	24	25	1	0.214	0.25
PRI_AN_DDH042	25	26	1	0.279	0.25
PRI_AN_DDH042	26	27	1	0.644	0.25
PRI_AN_DDH042	27	28	1	0.516	1
PRI_AN_DDH042	28	29	1	0.764	1
PRI_AN_DDH042	29	30	1	1.02	4
PRI_AN_DDH042	30	31	1	1.46	4
PRI_AN_DDH042	31	32	1	0.543	1
PRI_AN_DDH042	32	33	1	0.392	0.25
PRI_AN_DDH042	33	34	1	0.252	0.25
PRI_AN_DDH042	34	35	1	1.68	3
PRI_AN_DDH042	35	36	1	0.358	0.25
PRI_AN_DDH042	36	37	1	0.809	1
PRI_AN_DDH042	38	39	1	0.399	1
PRI_AN_DDH042	39	40	1	0.228	0.25
PRI_AN_DDH042	40.6	42	1.4	0.474	1
PRI_AN_DDH042	42	43	1	0.241	0.25
PRI_AN_DDH042	50	51	1	0.34	0.25
PRI_AN_DDH042	52	53	1	0.201	1

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
PRI_AN_DDH042	59	60	1	0.228	1
PRI_AN_DDH042	60	61	1	0.465	2
PRI_AN_DDH042	62	62.83	0.83	0.229	2
PRI_AN_DDH042	66	67.14	1.14	0.352	3
PRI_AN_DDH042	69	70	1	0.408	1
PRI_AN_DDH042	70	71	1	0.673	1
PRI_AN_DDH042	71	72	1	0.502	1
PRI_AN_DDH042	84	84.56	0.56	0.203	1
PRI_AN_DDH042	89	90	1	0.448	1
PRI_AN_DDH042	96	97	1	0.23	0.25
PRI_AN_DDH042	99	100	1	0.254	1
PRI_AN_DDH042	100	101	1	0.265	0.25
PRI_AN_DDH042	101	102	1	0.299	0.25
PRI_AN_DDH042	102	103	1	0.313	0.25
PRI_AN_DDH042	103	104	1	0.221	1
PRI_AN_DDH042	105	106	1	0.282	3
PRI_AN_DDH042	107	108	1	0.262	1
PRI_AN_DDH042	108	109	1	0.321	1
PRI_AN_DDH042	109	110	1	0.213	1
PRI_AN_DDH042	110	111	1	0.241	3
PRI_AN_DDH042	117	118	1	0.228	183
PRI_AN_DDH042	118	118.94	0.94	0.947	63
PRI_AN_DDH042	124	125	1	0.214	4
PRI_AN_DDH042	125	126	1	0.297	5
PRI_AN_DDH042	126	127	1	0.217	5
PRI_AN_DDH042	127	128	1	0.247	8
PRI_AN_DDH042	128	128.5	0.5	0.235	6
PRI_AN_DDH042	129	130.46	1.46	0.208	6
PRI_AN_DDH043	54.67	55.5	0.83	0.236	1
PRI_AN_DDH043	56.35	57	0.65	0.94	1
PRI_AN_DDH043	57	58	1	0.886	2
PRI_AN_DDH043	58	59	1	0.589	3
PRI_AN_DDH043	59	59.72	0.72	0.353	2
PRI_AN_DDH043	59.72	61	1.28	0.531	14
PRI_AN_DDH043	61	62	1	0.537	16
PRI_AN_DDH043	176	177	1	0.295	5
PRI_AN_DDH043	222	223	1	0.386	4
PRI_AN_DDH043	223	224	1	0.222	2
PRI_AN_DDH044	66.95	68.05	1.1	0.61	2
PRI_AN_DDH044	68.05	69	0.95	0.544	0.25
PRI_AN_DDH044	69	70	1	1.74	2
PRI_AN_DDH044	70	71	1	1.145	2
PRI_AN_DDH044	71	72	1	1.92	7
PRI_AN_DDH044	72	73	1	1.385	6
PRI_AN_DDH044	73	74	1	2.24	28
PRI_AN_DDH044	74	75	1	0.22	2
PRI_AN_DDH044	76	77	1	0.219	1
PRI_AN_DDH044	78	78.91	0.91	0.277	6
PRI_AN_DDH045	134.35	135.75	1.4	0.648	2
PRI_AN_DDH045	135.75	136.5	0.75	0.475	2
PRI_AN_DDH045	136.5	137.5	1	0.311	3
PRI_AN_DDH047	190	191	1	0.226	0.25
PRI_AN_DDH047	193	194	1	0.283	9
PRI_AN_DDH047	195	196	1	0.378	7
PRI_AN_DDH047	196	197	1	0.2	2
PRI_AN_DDH047	203	204	1	0.268	3

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
PRI_AN_DDH047	204	205	1	0.374	2
PRI_AN_DDH047	205	206	1	0.271	0.25
PRI_AN_DDH047	207	207.77	0.77	0.3	0.25
PRI_AN_DDH047	211	212.29	1.29	0.567	2
PRI_AN_DDH047	212.29	213	0.71	0.337	0.25
PRI_AN_DDH047	215	216	1	0.326	0.25
PRI_AN_DDH047	216	216.52	0.52	0.239	0.25
PRI_AN_DDH047	216.52	218	1.48	0.31	0.25
PRI_AN_DDH047	218	219.43	1.43	0.384	0.25
PRI_AN_DDH047	222	223.37	1.37	0.261	1
PRI_AN_DDH047	224.35	225	0.65	0.912	2
PRI_AN_DDH047	225	226	1	0.42	0.25
PRI_AN_DDH047	227	228	1	0.482	0.25
PRI_AN_DDH047	228	229	1	1.21	1
PRI_AN_DDH047	229	230	1	0.93	3
PRI_AN_DDH047	230	231	1	6.69	19
PRI_AN_DDH047	231	232	1	1.85	4
PRI_AN_DDH047	232	233	1	1.485	7
PRI_AN_DDH047	243.16	244	0.84	0.742	7
PRI_AN_DDH047	244	245	1	0.754	8
PRI_AN_DDH047	245	246.06	1.06	0.8	8
PRI_AN_DDH047	246.06	246.98	0.92	0.67	5
PRI_AN_DDH047	246.98	248	1.02	0.677	10
PRI_AN_DDH047	248	249	1	0.804	13
PRI_AN_DDH047	251	252	1	0.381	4
PRI_AN_DDH047	252	253	1	0.451	5
PRI_AN_DDH047	253	254	1	0.258	3
PRI_AN_DDH047	254	255	1	0.254	3
PRI_AN_DDH047	255	256	1	0.241	5
PRI_AN_DDH047	256	257	1	0.481	10
PRI_AN_DDH047	257	258	1	0.528	11
PRI_AN_DDH047	258	259	1	0.707	16
PRI_AN_DDH047	259	260	1	0.207	3
PRI_AN_DDH047	264	265	1	0.228	4
PRI_AN_DDH047	265	265.74	0.74	0.352	8
PRI_AN_DDH047	265.74	267	1.26	0.927	18
PRI_AN_DDH047	267	268	1	0.465	11
PRI_AN_DDH047	268	268.63	0.63	0.356	9
PRI_AN_DDH047	277	278.32	1.32	0.842	10
PRI_AN_DDH047	282.39	283	0.61	0.202	2
PRI_AN_DDH047	283	284	1	0.753	3
PRI_AN_DDH047	284	285	1	0.602	2
PRI_AN_DDH047	285	286	1	0.61	2
PRI_AN_DDH047	287	287.77	0.77	0.286	5
PRI_AN_DDH047	312.42	313	0.58	0.202	1
PRI_AN_DDH049	86.44	87.36	0.92	0.452	4
PRI_AN_DDH049	87.36	88	0.64	0.775	2
PRI_AN_DDH049	88	89	1	0.5	0.25
PRI_AN_DDH049	89	89.75	0.75	0.546	0.25
PRI_AN_DDH049	91	92	1	0.325	1
PRI_AN_DDH049	92	93	1	3.86	28
PRI_AN_DDH049	93	94	1	3.21	23
PRI_AN_DDH049	94	95	1	1.41	14
PRI_AN_DDH049	95	96	1	1.27	11
PRI_AN_DDH049	96	97	1	1.73	17
PRI_AN_DDH049	97	98	1	0.62	6

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
PRI_AN_DDH049	98	99	1	1.735	12
PRI_AN_DDH049	99	100	1	1.555	10
PRI_AN_DDH049	100	101.09	1.09	0.767	4
PRI_AN_DDH049	101.09	102	0.91	0.553	2
PRI_AN_DDH049	102	102.76	0.76	0.355	2
PRI_AN_DDH049	102.76	104	1.24	0.52	3
PRI_AN_DDH049	105	106	1	0.259	3
PRI_AN_DDH049	106	107.23	1.23	0.503	9
PRI_AN_DDH049	107.23	108	0.77	0.484	7
PRI_AN_DDH049	131	132	1	0.208	16
PRI_AN_DDH049	153.59	155	1.41	0.339	22
AND-19-002	106	117	11		
TRPA01	10	11	1	0.228	0.25
TRPA01	13	14	1	0.415	0.25
TRPA01	15	16	1	0.249	1.9
TRPA01	16	17	1	0.361	0.25
TRPA01	17	18	1	0.239	0.25
TRPA02	6	7	1	0.213	0.8
TRPA02	7	8	1	0.322	0.25
TRPA02	8	9	1	0.231	0.25
TRPA02	12.8	13.6	0.8	0.205	0.25
TRPA03	1.5	2.5	1	0.21	4.4
TRPA03	2.5	3.5	1	0.305	7.2
TRPA03	3.5	4.5	1	0.976	1.3
TRPA03	4.5	5.5	1	0.321	4.4
TRPA03	5.5	6.5	1	0.387	7.4
TRPA03	6.5	7.5	1	0.568	12.1
TRPA03	7.5	8.5	1	1.425	42.5
TRPA03	8.5	9.5	1	0.278	15.6
TRPA03	9.5	10	0.5	0.23	7.8
TRPA03	10	11	1	0.334	11.7
TRPA03	11	12	1	1.02	8.5
TRPA03	12	13	1	0.325	10.8
TRPA03	14	15	1	0.247	14.1
TRPA03	15	16	1	0.365	12.5
TRPA03	17	18	1	0.44	16.8
TRPA03	18	18.5	0.5	0.202	16.1
TRPA03	18.5	19.5	1	1.305	60.8
TRPA04	0	1	1	0.353	7.8
TRPA04	1	2	1	0.5	5.3
TRPA04	2	3	1	1.7	14
TRPA04	3	4	1	1.325	17.6
TRPA04	4	5	1	0.947	17.3
TRPA04	5	6	1	1.525	19.5
TRPA04	6	7	1	1.26	11.9
TRPA04	7	8	1	1.7	32
TRPA04	8	9	1	2.34	30.8
TRPA04	9	10	1	0.866	15.3
TRPA04	10	11	1	1.445	20.6
TRPA04	14	15	1	0.217	9.9
TRPA04	24.5	25.5	1	0.528	8.2
TRPA04	25.5	26	0.5	0.726	13.9
TRPA04	31	32	1	1.305	3.5
TRPA04	32	33	1	0.739	7.6
TRPA04	34	35	1	0.227	7.8
TRPA04	35	36	1	0.295	6.5

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
TRPA04	36	37	1	0.933	7.9
TRPA04	37	38	1	0.747	5.9
TRPA04	38	39	1	0.704	6.9
TRPA04	39	40	1	0.915	8
TRPA04	40	41	1	0.313	2.4
TRPA04	41	42	1	0.476	6.1
TRPA04	42	43	1	0.699	6.1
TRPA04	43	44	1	0.737	8.9
TRPA04	44	45	1	0.808	11.8
TRPA04	45	46	1	0.474	8.4
TRPA04	46	47	1	0.557	10.1
TRPA04	47	48	1	0.298	8.1
TRPA04	48	49	1	0.439	10.3
TRPA04	49	50	1	1.87	7.8
TRPA04	50	50.5	0.5	4.01	4
TRPA04	50.5	51.5	1	3.4	4.5
TRPA04	51.5	52.5	1	0.578	7.6
TRPA04	53.5	54.5	1	0.231	10
TRPA04	54.5	55.5	1	0.214	17.4
TRPA04	55.5	56.5	1	0.453	15
TRPA04	80.5	81.5	1	0.216	0.8
TRPA04	82.5	83.5	1	0.272	0.7
TRPA04	83.5	84.5	1	0.462	0.25
TRPA04	87.5	88.5	1	0.464	1.3
TRPA04	98.5	99.5	1	0.2	0.7
TRPA04	100.5	101.5	1	0.484	0.25
TRPA04	101.5	102.5	1	0.221	0.25
TRPA04	102.5	103.5	1	0.461	0.25
TRPA04	104.5	105.5	1	0.311	0.25
TRPA04	122.5	123.5	1	0.383	0.25
TRPA04	123.5	124.5	1	0.815	0.25
TRPA04	126.5	127.5	1	0.334	0.25
TRPA04	145.5	146.5	1	0.208	0.25
TRPA05	23	24	1	0.555	11.2
TRPA05	24	25	1	1.17	27.7
TRPA05	25	26	1	0.522	16.4
TRPA05	26	27	1	2.53	25.8
TRPA05	27	28	1	0.443	17.7
TRPA05	28	29	1	0.689	9.4
TRPA05	29	30	1	0.579	8.6
TRPA05	30	31	1	0.444	11.1
TRPA05	31	32	1	0.791	9.1
TRPA05	32	33	1	0.485	6.7
TRPA05	33	34	1	0.349	6.7
TRPA05	34	35	1	0.376	3.8
TRPA05	35	36	1	0.645	5.9
TRPA05	36	37	1	0.305	0.25
TRPA05	37	38	1	0.442	3.8
TRPA05	38	39	1	0.293	1.2
TRPA05	39	40	1	0.223	2.3
TRPA05	40	41	1	0.505	5
TRPA05	41	42	1	0.487	1.6
TRPA05	42	43	1	0.246	2.3
TRPA05	43	44	1	0.387	2.6
TRPA06	0	1	1	0.452	7.1
TRPA06	1	2	1	1.37	5.8

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
TRPA06	2	3	1	0.919	5
TRPA06	3	4	1	0.435	5.9
TRPA06	4	5	1	1.14	8.4
TRPA06	5	6	1	1.705	12.9
TRPA06	6	7	1	0.79	1.9
TRPA06	7	8	1	0.508	2.5
TRPA06	8	9	1	0.649	1.4
TRPA06	9	10	1	0.511	2.6
TRPA06	10	11	1	0.382	2
TRPA06	11	12	1	0.392	2.4
TRPA06	12	13	1	0.505	3.1
TRPA06	13	14	1	0.247	2.4
TRPA06	14	15	1	0.568	3.8
TRPA06	15	16	1	0.245	2.4
TRPA06	17.5	18.5	1	0.508	1.9
TRPA06	18.5	19.5	1	0.332	2.1
TRPA06	19.5	20.5	1	0.204	2.2
TRPA06	21.5	22.5	1	0.364	3.1
TRPA06	22.5	23.5	1	0.231	3.5
TRPA06	24.5	25.5	1	0.211	3.8
TRPA06	33.5	34.5	1	0.223	5.6
TRPA07	19.5	20.5	1	0.268	2.6
TRPA07	20.5	21.5	1	0.346	3.4
TRPA07	21.5	22.5	1	0.527	4.2
TRPA07	22.5	23.5	1	0.58	1.7
TRPA07	23.5	24.5	1	0.687	3.3
TRPA07	24.5	25.5	1	2.32	11.4
TRPA07	25.5	26.5	1	0.207	12
TRPA07	26.5	27.5	1	0.267	7.9
TRPA07	27.5	28.5	1	0.511	4.6
TRPA07	28.5	29.5	1	0.687	1.7
TRPA07	29.5	30.5	1	0.428	4.5
TRPA07	30.5	31	0.5	0.292	2.6
TRPA07	31	32	1	0.235	2.5
TRPA07	32	33	1	0.303	1.6
TRPA07	33	34	1	0.281	0.25
TRPA07	34	35	1	0.306	0.7
TRPA07	35	36	1	0.285	0.25
TRPA07	37	38	1	0.221	1.5
TRPA07	38	39	1	0.236	1.6
TRPA07	39	40	1	0.217	2.3
TRPA07	56	57	1	0.314	3.5
TRPA07	58	59	1	0.228	5.5
TRPA07	68	69	1	0.221	2.3
TRPA07	69	70	1	0.388	3.2
TRPA07	78	79	1	0.29	1.5
TRPA07	79	80	1	0.409	1.7
TRPA07	87	88	1	0.336	0.9
TRPA07	88	89	1	0.214	0.8
TRPA07	89	90	1	0.296	0.6
TRPA07	90	91	1	0.214	0.25
TRPA07	91	92	1	0.607	0.25
TRPA07	92	93	1	0.854	0.25
TRPA07	93	94	1	1.775	0.25
TRPA07	94	95	1	0.44	1.7
TRPA07	95	96	1	0.49	0.9

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
TRPA07	96	97	1	0.379	2
TRPA07	97	98	1	0.254	1
TRPA07	98	99	1	0.477	0.6
TRPA07	99	100	1	0.283	1.4
TRPA07	117	118	1	0.226	0.25
TRPA07	120	121	1	0.255	0.6
TRPA07	121	122	1	0.407	0.25
TRPA07	122	123	1	0.316	0.9
TRPA07	123	123.5	0.5	0.524	0.25
TRPA07	123.5	124.5	1	0.27	1.4
TRPA07	124.5	125.5	1	0.257	2.9
TRPA07	125.5	126.5	1	0.219	2
TRPA07	126.5	127.5	1	0.281	2.3
TRPA07	127.5	128.5	1	0.261	1.7
TRPA07	128.5	129.5	1	1.275	0.6
TRPA07	129.5	130.5	1	0.462	0.25
TRPA07	130.5	131.5	1	0.343	0.6
TRPA07	131.5	132.5	1	0.425	0.25
TRPA07	132.5	133.5	1	0.433	0.25
TRPA07	133.5	134.5	1	0.214	0.8
TRPA07	134.5	135.5	1	0.246	0.25
TRPA07	135.5	136.5	1	0.341	0.25
TRPA07	136.5	137.5	1	0.654	1.2
TRPA07	137.5	138	0.5	0.395	0.25
TRPA07	138	139	1	0.274	4.7
TRPA07	139	140	1	0.282	5
TRPA07	140	141	1	0.745	4.9
TRPA07	141	142	1	0.595	0.9
TRPA07	142	143	1	0.29	0.7
TRPA07	143	144	1	0.333	0.6
TRPA07	144	145	1	2.04	8.5
TRPA07	146	147	1	0.506	0.7
TRPA07	148	149	1	0.204	5.4
TRPA07	149	150	1	0.353	5
TRPA07	151	152	1	0.308	10
TRPA07	152	153	1	0.851	9.7
TRPA07	153	154	1	0.246	10.6
TRPA07	157	158	1	0.233	1.2
TRPA07	158	159	1	0.335	2.3
TRPA08	0	1	1	0.292	3.9
TRPA08	1	2	1	0.408	4.5
TRPA08	2	3	1	0.5	4
TRPA08	3	4	1	0.439	4.3
TRPA08	4	5	1	0.258	4.3
TRPA08	5	6	1	0.555	6.4
TRPA08	6	7	1	0.221	4.1
TRPA08	7	8	1	0.328	5.4
TRPA08	8	9	1	0.239	4.6
TRPA08	9	10	1	0.309	4.9
TRPA08	10	11	1	0.332	4.1
TRPA08	11	11.5	0.5	0.347	5.8
TRPA08	11.5	12.5	1	0.323	4.1
TRPA08	12.5	13.5	1	0.415	3.2
TRPA08	13.5	14.5	1	0.466	5.3
TRPA08	14.5	15.5	1	0.347	4.5
TRPA08	15.5	16.5	1	0.3	1.7

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
TRPA08	16.5	17.5	1	0.29	0.9
TRPA08	17.5	18.5	1	0.284	0.25
TRPA08	18.5	19.5	1	0.253	0.25
TRPA08	19.5	20.5	1	0.218	0.25
TRPA08	20.5	21.5	1	0.21	0.25
TRPA08	21.5	22.5	1	0.358	0.25
TRPA08	22.5	23.5	1	0.307	0.25
TRPA08	23.5	24.5	1	0.207	0.25
TRPA08	24.5	25.5	1	0.206	3.2
TRPA08	25.5	26.5	1	0.211	7
TRPA08	34.5	35.5	1	0.207	4
TRPA08	35.5	36.5	1	0.219	3.6
TRPA08	36.5	37.5	1	0.225	2.1
TRPA08	39.5	40.5	1	0.286	0.7
TRPA08	40.5	41.5	1	0.65	1.3
TRPA08	41.5	42.5	1	0.544	3.5
TRPA08	42.5	43.5	1	0.744	3.5
TRPA08	43.5	44.5	1	0.702	6.6
TRPA08	44.5	45.5	1	0.564	10.8
TRPA08	45.5	46.5	1	0.829	9
TRPA08	46.5	47.5	1	0.244	4.6
TRPA09	1	2	1	0.611	3.2
TRPA09	3	4	1	0.485	1.9
TRPA09	4	5	1	0.372	2.4
TRPA09	5	6	1	0.354	0.7
TRPA09	6	7	1	0.455	2
TRPA09	9	10	1	0.351	2.8
TRPA09	14	15	1	0.635	1.1
TRPA09	18	19	1	0.221	1.4
TRPA09	19	20	1	0.221	1.6
TRPA09	25	26	1	0.204	3.9
TRPA09	26	27	1	0.387	3.2
TRPA09	27	28	1	0.313	5
TRPA10	0	1	1	0.466	0.25
TRPA10	1	2	1	0.239	1.3
TRPA10	2	3	1	0.486	1.7
TRPA10	3	4	1	0.289	0.9
TRPA10	4	5	1	0.372	0.7
TRPA10	5	6	1	2.95	0.25
TRPA10	6	7	1	0.293	1.3
TRPA10	7	8	1	0.439	1
TRPA10	8	9	1	0.209	1.1
TRPA10	9	10	1	0.288	1.5
TRPA10	10	11	1	0.999	2.5
TRPA10	11	12	1	0.419	0.9
TRPA10	12	13	1	0.279	0.9
TRPA10	13	14	1	0.892	1.9
TRPA10	14	15	1	1.51	0.7
TRPA10	15	16	1	1.45	0.25
TRPA10	16	17	1	0.584	0.25
TRPA10	18	19	1	0.444	1.7
TRPA10	19	20	1	0.869	2.3
TRPA10	20	21	1	0.853	1.4
TRPA10	21	22	1	0.355	1
TRPA10	22	23	1	1.725	2.8
TRPA10	23	24	1	0.397	1

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
TRPA10	24	25	1	1.25	0.25
TRPA10	25	26	1	0.493	0.8
TRPA10	26	27	1	0.54	0.7
TRPA10	27	28	1	0.658	3.2
TRPA10	28	29	1	0.693	3.6
TRPA10	29	30	1	0.309	2.9
TRPA11	0	1	1	0.302	2
TRPA11	3	4	1	0.468	1.4
TRPA11	5	6	1	0.267	1.2
TRPA11	6	7	1	0.241	0.25
TRPA11	7	8	1	0.389	1.5
TRPA11	8	9	1	0.259	1.8
TRPA11	9	10	1	0.237	0.9
TRPA11	11	12	1	0.281	1.7
TRPA11	14	14.5	0.5	0.26	0.7
TRPA11	18.5	19.5	1	0.271	0.7
TRPA11	19.5	20.5	1	0.271	1.8
TRPA11	21.5	22.5	1	0.377	1.6
TRPA11	22.5	23.5	1	0.434	1.4
TRPA11	23.5	24.5	1	0.212	1.1
TRPA11	27.5	28.5	1	0.355	1.2
TRPA11	28.5	29.5	1	0.247	1.1
TRPA11	29.5	30.5	1	0.491	1.1
TRPA11	30.5	31.5	1	0.341	1.8
TRPA11	31.5	32.5	1	0.307	2.4
TRPA11	32.5	33.5	1	1.57	5.6
TRPA11	35.5	36.5	1	0.302	2.4
TRPA11	36.5	37.5	1	0.635	2.3
TRPA11	37.5	38.5	1	0.265	1.9
TRPA11	38.5	39.5	1	0.861	1.3
TRPA11	39.5	40.5	1	1.02	2.7
TRPA13	8	9	1	0.273	1.2
TRPA13	9	10	1	0.362	3.4
TRPA13	19	20	1	0.232	1.5
TRPA13	20	21	1	0.524	1.5
TRPA13	21	22	1	0.463	0.25
TRPA13	22	23	1	0.568	0.9
TRPA13	23	24	1	0.478	0.8
TRPA13	25	26	1	0.233	1.2
TRPA13	26	27	1	1.035	1.7
TRPA13	28	29	1	0.655	1.7
TRPA13	29	30	1	0.597	2.2
TRPA13	32	33	1	0.356	0.8
TRPA13	34	35	1	0.246	0.7
TRPA13	35	36	1	0.231	0.7
TRPA13	37	38	1	0.555	1.7
TRPA13	38	39	1	0.37	1.2
TRPA13	39	40	1	0.226	0.8
TRPA13	40	41	1	0.503	2.7
TRPA13	42	43	1	0.318	2.2
TRPA13	44	45	1	0.503	1.6
TRPA13	45	46	1	0.363	1.5
TRPA13	47	48	1	0.38	1.2
TRPA13	48	49	1	0.349	0.6
TRPA13	51	52	1	0.589	1
TRPA13	54	55	1	0.372	1.2

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
TRPA13	56	57	1	0.705	0.6
TRPA13	57	58	1	0.288	0.9
TRPA13	58	59	1	0.55	2.1
TRPA13	59	60	1	0.37	2.7
TRPA13	61	62	1	0.267	0.9
TRPA13	62	63	1	0.234	0.6
TRPA13	63	64	1	0.43	0.6
TRPA13	64	65	1	0.263	0.8
TRPA14	0	1	1	0.426	1.9
TRPA14	1	2	1	0.396	2
TRPA14	2	3	1	0.575	1.4
TRPA14	3	4	1	1.35	1.7
TRPA14	4	5	1	1.325	0.8
TRPA14	5	6	1	1.8	0.6
TRPA14	6	7	1	0.743	1.9
TRPA14	7	7.5	0.5	0.669	2.1
TRPA14	7.5	8.5	1	0.38	2.7
TRPA14	8.5	9.5	1	0.586	1.9
TRPA14	9.5	10.5	1	0.394	3.2
TRPA14	10.5	11.5	1	0.595	4
TRPA14	11.5	12.5	1	0.612	6
TRPA14	12.5	13.5	1	1.275	6.6
TRPA14	13.5	14.5	1	0.525	3.1
TRPA14	14.5	15.5	1	0.213	0.25
TRPA14	15.5	16.5	1	0.91	5.7
TRPA14	16.5	17.5	1	0.626	2.8
TRPA14	17.5	18.5	1	2.57	14.2
TRPA14	35.5	36.5	1	0.268	3
TRPA14	41.5	42.5	1	0.98	8.1
TRPA14	42.5	43.5	1	0.327	0.9
TRPA14	43.5	44.5	1	0.482	1.1
TRPA14	44.5	45.5	1	0.821	1.5
TRPA14	45.5	46.5	1	0.629	3.7
TRPA14	47.5	48.5	1	0.29	0.7
TRPA14	52.5	53.5	1	0.316	0.25
TRPA14	53.5	54.5	1	0.283	0.25
TRPA14	55.5	56.5	1	0.339	2
TRPA14	56.5	57.5	1	0.369	2.6
TRPA14	58.5	59.5	1	0.223	2
TRPA14	60.5	61.5	1	0.254	4.3
TRPA14	64.5	65.5	1	1.925	0.25
TRPA14	65.5	66.5	1	0.519	0.25
TRPA14	66.5	67.5	1	0.254	0.7
TRPA14	68.5	69.5	1	0.274	0.25
TRPA14	69.5	70.5	1	0.203	0.25
TRPA14	94	95	1	0.237	1.5
TRPA14	100	101	1	0.249	0.7
TRPA14	105	106	1	0.253	0.25
TRPA15	1	2	1	0.204	1.1
TRPA15	2	3	1	0.373	2.1
TRPA15	7	8	1	0.235	1.4
TRPA15	8	9	1	0.448	1.5
TRPA15	9	9.8	0.8	0.528	2.3
TRPA15	9.8	10.8	1	0.584	1.3
TRPA15	24.6	25.6	1	0.249	2.4
TRPA15	25.6	26.6	1	0.241	2.3

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
TRPA15	26.6	27.6	1	0.202	3.4
TRPA15	27.6	28.6	1	0.28	3.2
TRPA15	28.6	29.6	1	0.238	3.3
TRPA15	29.6	30.6	1	0.289	3.4
TRPA15	31.6	32.6	1	0.359	1.4
TRPA16	7	8	1	0.408	1.2
TRPA16	8	9	1	0.261	0.6
TRPA17	2	3	1	0.267	8.2
TRPA17	28	29	1	0.286	16.9
TRPA17	29	30	1	0.285	6.5
TRPR06	11	12	1	0.201	1.5
TRPR07	9.6	10	0.4	0.366	0.9
TRPR07	10	11	1	0.223	2.6
TRPR07	11	12	1	0.836	0.7
TRPR07	12	13	1	0.236	0.25
TRPR07	13	14	1	1.45	1.4
TRPR07	14	15	1	1.455	2.5
TRPR07	15	16	1	1.6	2.6
TRPR07	16	17	1	1.205	1.3
TRPR07	17	18	1	0.401	0.25
TRPR07	18	19	1	0.358	0.25
TRPR08	5	6	1	0.223	0.6
TRPR08	9.5	10.5	1	0.275	2
TRPR08	10.5	11.5	1	0.802	5.2
TRPR08	11.5	12.5	1	0.234	3.5
TRPR08	12.5	13.5	1	0.313	21.4
TRPR09	0	1	1	0.557	4.9
TRPR09	1	2	1	0.621	4
TRPR09	2	3	1	0.247	6.4
TRPR09	4	5	1	0.313	8
TRPR09	5	6	1	0.422	8.8
TRPR09	6	7	1	0.378	12.6
TRPR09	7	8	1	0.24	8.7
TRPR09	8	9	1	0.282	8.9
TRPR09	9	10	1	0.231	4.3
TRPR09	10	11	1	0.246	2.4
TRPR09	11	12	1	0.674	5.5
TRPR09	12	13	1	0.998	45.3
TRPR09	13	14	1	0.29	6.6
TRPR09	14	15	1	0.294	3.6
TRPR09	15	15.5	0.5	0.408	3.9
TRPR09	15.5	16.5	1	0.529	4.9
TRPR09	16.5	17.5	1	0.31	4.1
TRPR09	17.5	18	0.5	0.331	4.4
TRPR09	18	19	1	0.328	3.1
TRPR09	19	19.5	0.5	0.211	4.5
TRPR09	19.5	20.5	1	0.385	1.3
TRPR09	20.5	21.5	1	0.411	3.2
TRPR09	21.5	22	0.5	0.64	8.7
TRPR09	22	23	1	0.61	13.4
TRPR09	23	24	1	0.518	1.2
TRPR09	25	26	1	0.217	0.8
TRPR10	5	6	1	0.52	1.1
TRPR10	6	7	1	0.3	2.5
TRPR10	7	8	1	0.314	3.2
TRPR10	8	8.5	0.5	0.367	3

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
TRPR10	8.5	9.5	1	1.415	2
TRPR10	9.5	10.5	1	0.634	2.5
TRPR11	3	4	1	0.402	1.7
TRPR11	4	5	1	0.208	1.2
TRPR11	5	6	1	0.209	5.8
TRPR11	7	8	1	0.202	3.3
TRPR11	8	9	1	0.223	4.6
TRPR11	9	10	1	0.233	5.3
TRPR11	10	11	1	0.295	2.6
TRPR11	11	12	1	0.257	2.4
TRPR11	12	13	1	0.351	2.3
TRPR11	13	14	1	0.326	2.4
TRPR11	14	15	1	0.498	2.1
TRPR11	15	16	1	0.942	3.2
TRPR11	16	17	1	0.995	17.3
TRPR11	17	18	1	0.434	3.7
TRPR11	18	19	1	0.539	5.1
TRPR11	19	20	1	0.743	4.6
TRPR11	20	21	1	0.45	2.5
TRPR11	21	22	1	0.598	2
TRPR11	22	23	1	1.015	4.5
TRPR11	23	24	1	0.596	0.25
TRPR11	24	25	1	0.302	0.7
TRPR11	25	26	1	0.916	4.5
TRPR11	26	27	1	0.924	2.2
TRPR11	27	28	1	0.864	3.5
TRPR11	28	29	1	1.4	5.2
TRPR11	29	30	1	0.205	1
TRPR11	32	33	1	0.229	0.7
TRPR11	34	35	1	0.278	1.8
TRPR11	35	36	1	0.506	3.7
TRPR11	36	37	1	0.283	2
TRPR11	37	38	1	4.68	43.2
TRPR11	38	39	1	0.27	5.6
TRPR11	39	40	1	1.225	24.4
TRPR11	40	41.2	1.2	0.71	16.1
TRPR11	41.2	42.2	1	0.27	4.7
TRPR11	42.2	43.2	1	2.75	16.6
TRPR11	43.2	44.2	1	6.15	22.9
TRPR11	44.2	45.2	1	4.52	10.9
TRPR11	45.2	46.2	1	3.96	8
TRPR11	46.2	47.2	1	1.49	3.6
TRPR11	47.2	48.2	1	0.887	1.9
TRPR11	48.2	49.2	1	1.945	4.9
TRPR11	49.2	50.2	1	0.363	3.4
TRPR11	50.2	51.5	1.3	2.98	9.8
TRPR11	51.5	52.5	1	1.38	8.2
TRPR11	52.5	53.5	1	1.275	12
TRPR11	53.5	54.5	1	1.24	11.1
TRPR11	54.5	55	0.5	0.269	5.7
TRPR11	87	88	1	0.393	0.8
TRPR11	88	89	1	0.296	0.6
TRPR11	93	94	1	0.269	0.8
TRPR11	94	95	1	0.241	0.25
TRPR11	95	96	1	0.294	0.25
TRPR11	96	97	1	0.465	0.25

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
TRPR11	97	98	1	0.635	0.25
TRPR11	98	99	1	0.579	0.6
TRPR11	99	100	1	0.896	0.6
TRPR11	100	101	1	0.936	0.7
TRPR11	101	102	1	0.374	0.25
TRPR11	102	103	1	2.13	1
TRPR11	103	104	1	1.1	0.25
TRPR11	104	105	1	2.23	1.1
TRPR11	105	106	1	2.29	1
TRPR11	106	107	1	0.952	0.25
TRPR11	107	108	1	1.07	0.7
TRPR11	108	109	1	0.764	1.5
TRPR11	109	110	1	0.771	1.1
TRPR11	110	111	1	1.13	1
TRPR11	111	112	1	2.59	4.2
TRPR11	112	113	1	1.4	2
TRPR11	113	114	1	1.165	4.7
TRPR11	114	115	1	0.696	1.6
TRPR11	115	116	1	0.26	0.6
TRPR11	117	118	1	0.279	0.25
TRPR11	119	120	1	0.259	0.6
TRPR11	120	121	1	0.254	0.25
TRPR11	121	122	1	0.263	0.25
TRPR13	0	1	1	2.59	25.7
TRPR13	1	2	1	2.03	23.6
TRPR13	2	3	1	1.195	25.1
TRPR13	3	4	1	1.445	21.5
TRPR13	4	5	1	0.222	14.7
TRPR13	7	8	1	0.564	21
TRPR13	8	9	1	0.776	25.2
TRPR13	9	10	1	0.878	38.3
TRPR13	10	11	1	2.72	55.2
TRPR14	2.65	3.3	0.65	0.938	2.7
TRPR14	3.3	4.3	1	0.778	18
TRPR14	4.3	5.3	1	0.989	15.3
TRPR14	5.3	6.3	1	0.85	4.2
TRPR14	6.3	7.3	1	0.513	0.25
TRPR15	6	7	1	0.522	0.25
TRPR15	7	8	1	0.448	26.7
TRPR15	8	9	1	0.915	27.2
TRPR15	9	10	1	2.07	16.4
TRPR15	10	11	1	0.509	11.4
TRPR15	11	12	1	2.61	6
TRPR15	12	13	1	0.521	5.3
TRPR15	13	14	1	1.625	7
TRPR15	14	15	1	0.888	3.5
TRPR15	15	16	1	0.411	0.25
TRPR15	16	17	1	0.595	0.6
TRPR15	17	18	1	0.455	0.8
TRPR15	18	19	1	0.215	0.25
TRPR15	21.5	22.5	1	0.249	0.25
TRPR15	82.5	83.5	1	0.245	0.25
TRPR15	83.5	84.5	1	0.359	0.25
TRPR15	130.5	131.5	1	0.321	2
TRPR15	131.5	132.5	1	0.268	4.4
TRPR15	137.5	138.5	1	0.427	1.6

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
TRPR15	138.5	139.5	1	0.377	1.5
TRPR15	139.5	140.5	1	0.969	1.9
TRPR15	140.5	141.5	1	0.963	0.9
TRPR15	141.5	142.5	1	0.48	0.7
TRPR15	142.5	143.5	1	0.408	0.25
TRPR15	143.5	144.5	1	0.36	0.25
TRPR15	144.5	145.5	1	0.431	0.6
TRPR15	145.5	146.5	1	0.646	0.25
TRPR15	146.5	147.5	1	0.665	0.6
TRPR15	147.5	148.5	1	1.79	1.4
TRPR15	148.5	149.5	1	1.535	2.2
TRPR15	149.5	150.5	1	0.843	1.8
TRPR15	150.5	151.5	1	2.1	2.2
TRPR15	151.5	152.5	1	0.675	2
TRPR15	152.5	153.5	1	0.906	3.5
TRPR15	153.5	154.5	1	0.415	3.5
TRPR15	154.5	155.5	1	0.289	5.7
TRPR16	0	1	1	0.334	4.3
TRPR16	1	2	1	0.24	4.3
TRPR16	2	3	1	0.51	4.7
TRPR16	3	4	1	1.135	5
TRPR16	4	5	1	0.462	3.3
TRPR16	5	6	1	0.236	2
TRPR16	6	7	1	0.818	0.8
TRPR16	8	9	1	0.22	1.6
TRPR16	9	9.85	0.85	0.39	0.25
TRPR17	5.8	6.8	1	0.209	4.8
TRPR18	0	1	1	0.249	0.25
TRPR18	1	2	1	0.471	0.25
TRPR18	2	3	1	0.375	0.25
TRPR18	5	6	1	0.256	0.25
TRPR18	7	8	1	0.449	9.6
TRPR19	0	1	1	0.295	1.3
TRPR19	1	2	1	0.269	0.7
TRPR19	2	3	1	0.421	0.7
TRPR19	3	4	1	0.949	1.4
TRPR19	4	5	1	0.9	2.5
TRPR19	5	6	1	0.653	1.5
TRPR20	0	1	1	0.269	0.25
TRPR20	1	2	1	0.333	0.25
TRPR20	2	3	1	0.517	1.8
TRPR20	3	4	1	0.299	1.9
TRPR21A	1	2	1	0.488	1.9
TRPR21A	2	3	1	0.476	3.9
TRPR25	3	4	1	0.232	0.25
TRPR25	6	7	1	0.335	0.25
TRPR25	7	8	1	0.307	0.25
TRPR25	8	9	1	0.389	0.25
TRPR25	9	10	1	0.404	0.9
TRPR25	10	11	1	0.2	0.25
TRPR25	11	12	1	0.247	0.25
TRPR25	13	14	1	0.382	0.25
TRPR25	14	14.5	0.5	0.505	0.25
TRPR25	14.5	15.5	1	0.285	0.25
TRPR25	15.5	16	0.5	0.206	0.25
TRPR25	16	17	1	0.212	0.25

HOLE-ID	FROM	TO	LENGTH	CU%	AGPPM
TRPR25	18	19	1	0.409	1.8
TRPR25	19	20	1	0.229	2
TRPR25	20	21	1	0.273	2.5
GALERYAN	0	1	1	1.18	16.7
GALERYAN	1	2	1	0.473	8.8
GALERYAN	2	3	1	0.765	13.1
GALERYAN	3	4	1	0.884	18.2
GALERYAN	4	5	1	0.965	9.9
GALERYAN	5	6	1	1.325	14.5
GALERYAN	6	7	1	1.255	14
GALERYAN	7	8	1	0.825	11.6
GALERYAN	8	9	1	0.76	13
GALERYAN	9	10	1	1.68	19.3
GALERYAN	11	12	1	0.613	11.4
GALERYAN	12	13	1	0.353	6.4
GALERYAN	13	14	1	0.317	5.1
GALERYAN	16	17	1	0.614	10.6
GALERYAN	17	18	1	0.567	10.5
GALERYAN	18	19	1	0.346	9.3
GALERYAN	19	20	1	0.223	9.7
GALERYAN	21	22	1	0.456	15.1
GALERYAN	22	23.4	1.4	0.689	24.9